



دانشگاه کردستان
University of Kurdistan
زانکوی کوردستان

Nonlinear Analysis of Structures

Geometrically Nonlinear Analysis of Plane Trusses

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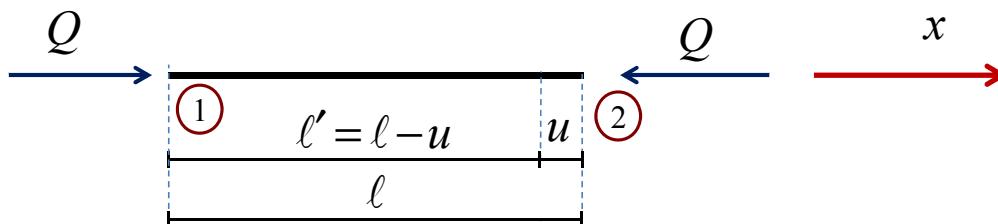
Geometrically Nonlinear Analysis of Plane Trusses

Member, Force-Deformation Relationship in local Coordinate

الف - روابط نیرو تغییر شکل در دستگاه مختصات محلی



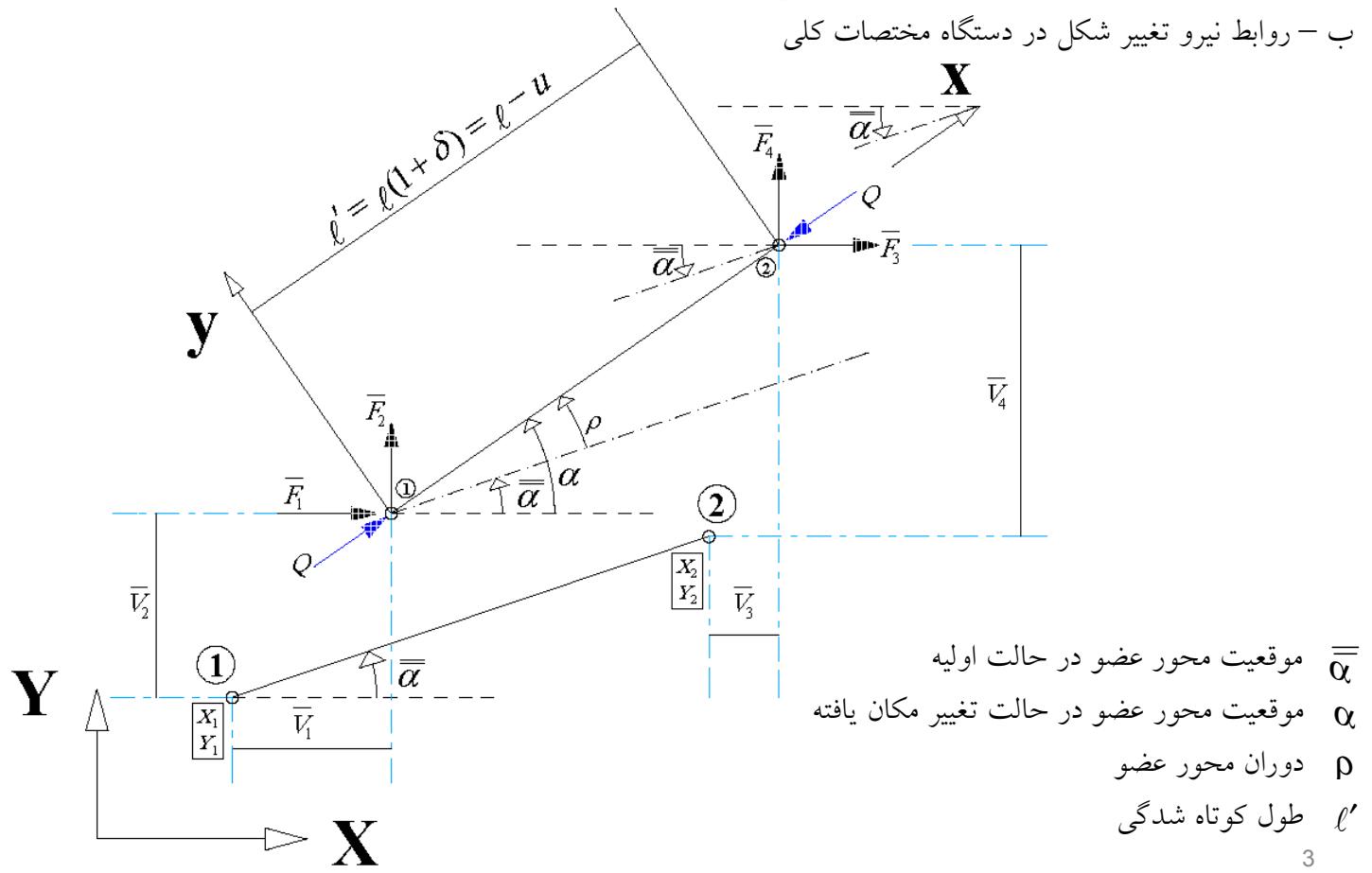
فرض انحنای کوچک برای خرپا لازم نیست



$$Q = \frac{AE}{l} u \quad (1)$$

Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate



Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate

$$\{\bar{F}\}_{4 \times 1} = [\bar{B}]_{4 \times 1} Q \quad (2)$$

نیروها در دستگاه مختصات کلی از رابطه زیر به دست می‌آید.

که در آن

$$\{\bar{F}\} = \begin{pmatrix} \bar{F}_1 \\ \bar{F}_2 \\ \bar{F}_3 \\ \bar{F}_4 \end{pmatrix}$$

نیروهای داخلی در دستگاه کلی $\{\bar{F}\}$

$$[\bar{B}] = \begin{bmatrix} m & \\ n & \\ -m & \\ -n & \end{bmatrix}, \quad m = \cos \alpha, \quad n = \sin \alpha \quad (3)$$

ماتریس انتقال $[\bar{B}]$ (Transformation Matrix)

$$u = \ell - \ell'$$

با توجه به شکل

$$\ell' = \left[((X_2 + \bar{V}_3) - (X_1 + \bar{V}_1))^2 + ((Y_2 + \bar{V}_4) - (Y_1 + \bar{V}_2))^2 \right]^{\frac{1}{2}} \quad (4)$$

$$m = \frac{(X_2 + \bar{V}_3) - (X_1 + \bar{V}_1)}{\ell'}, \quad n = \frac{(Y_2 + \bar{V}_4) - (Y_1 + \bar{V}_2)}{\ell'}$$

Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate

$$\{\Delta \bar{F}\} = [T] \{\Delta \bar{V}\} \quad (5)$$

$$[T] = \left[\frac{\partial \bar{F}_i^{(i)}}{\partial \bar{V}_j} \right]$$

M.T.S.M in Global Coordinate

که در آن

مشتق \bar{F}_i نسبت به هر یک از درجات آزادی $\frac{\partial \bar{F}_i^{(i)}}{\partial \bar{V}_j}$

$$\{\bar{V}\}_{4 \times 1} = \begin{Bmatrix} \bar{V}_1 \\ \bar{V}_2 \\ \bar{V}_3 \\ \bar{V}_4 \end{Bmatrix}$$

تغییر مکان گره‌ای در دستگاه کلی $\{\bar{V}\}$

شیوه $[t]$ در قاب‌ها است

$$[T] = \frac{AE}{\ell} [\bar{B}] [\bar{B}]^T + Q[g]$$

(6)

M.T.S.M in Global Coordinate

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Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate

$$[g] = \frac{1}{\ell'} \begin{bmatrix} -n^2 & mn & n^2 & -mn \\ mn & -m^2 & -mn & m^2 \\ n^2 & -mn & -n^2 & mn \\ -mn & m^2 & mn & -m^2 \end{bmatrix} \quad (7)$$

$$[\bar{B}] [\bar{B}]^T = \begin{bmatrix} m^2 & mn & -m^2 & -mn \\ mn & n^2 & -mn & -n^2 \\ -m^2 & -mn & m^2 & mn \\ -mn & -n^2 & mn & n^2 \end{bmatrix} \quad (8)$$

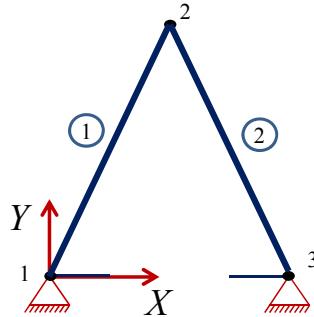
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Geometrically Nonlinear Analysis of Plane Trusses

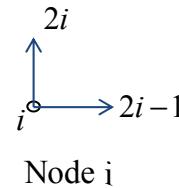
□ Member, Force-Deformation Relationship in Global Coordinate

مراحل

$$\{\Delta P\} = [\tau] \{\Delta x\}$$



۱) مختصات کلی تعیین می‌گردد (X,Y)



۲) شماره‌گذاری اعضای

۳) T برای هر عضو به کمک رابطه (6) محاسبه می‌شود.
۴) [τ] به کمک Assemble کردن تمام T ها به دست می‌آید.

$$[T^{(1)}] = \begin{bmatrix} 1 & 2 & 3 & 4 & 1 \\ & & & & 2 \\ & & & & 3 \\ & & & & 4 \end{bmatrix} \quad [T^{(2)}] = \begin{bmatrix} 3 & 4 & 5 & 6 & 3 \\ & & & & 4 \\ & & & & 5 \\ & & & & 6 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate

$$[\tau] = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 \\ T_{11}^{(1)} & T_{12}^{(1)} & T_{13}^{(1)} & T_{14}^{(1)} & 0 & 0 \\ T_{21}^{(1)} & T_{22}^{(1)} & T_{23}^{(1)} & T_{24}^{(1)} & 0 & 0 \\ T_{31}^{(1)} & T_{32}^{(1)} & T_{33}^{(1)} + T_{33}^{(2)} & T_{34}^{(1)} + T_{34}^{(2)} & T_{35}^{(2)} & T_{36}^{(2)} \\ T_{41}^{(1)} & T_{42}^{(1)} & T_{43}^{(1)} + T_{43}^{(2)} & T_{44}^{(1)} + T_{44}^{(2)} & T_{45}^{(2)} & T_{45}^{(2)} \\ 0 & 0 & T_{53}^{(2)} & T_{54}^{(2)} & T_{55}^{(2)} & T_{55}^{(2)} \\ 0 & 0 & T_{63}^{(2)} & T_{64}^{(2)} & T_{65}^{(2)} & T_{65}^{(2)} \end{bmatrix}$$

$$\{\Delta P\}_{6 \times 1} = [\tau]_{6 \times 6} \{\Delta x\}_{6 \times 1} \Rightarrow \left\{ \begin{array}{c} \{\Delta P\}_{2 \times 1} \\ \{\Delta R\}_{4 \times 1} \end{array} \right\}_{6 \times 1}^{\begin{array}{c} 3 \\ 4 \\ 1 \\ 2 \\ 5 \\ 6 \end{array}} = \left[\begin{array}{cc} \begin{bmatrix} 3 & 4 \\ 1 & 2 \end{bmatrix}_{2 \times 2} & \begin{bmatrix} 5 & 6 \\ 3 & 4 \end{bmatrix}_{2 \times 2} \\ \begin{bmatrix} \tau_{PP} \\ \tau_{PR} \end{bmatrix}_{4 \times 2} & \begin{bmatrix} \tau_{RP} \\ \tau_{RR} \end{bmatrix}_{4 \times 4} \end{array} \right]_{6 \times 6} \left\{ \begin{array}{c} \{\Delta x\}_{2 \times 1} \\ \{\Delta x_{Support}\}_{4 \times 1} \end{array} \right\}_{6 \times 1}^{\begin{array}{c} 3 \\ 4 \\ 1 \\ 2 \\ 5 \\ 6 \end{array}}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Member, Force-Deformation Relationship in Global Coordinate

$$\begin{Bmatrix} \{\Delta P\}_{2 \times 1} \\ \{\Delta R\}_{4 \times 1} \end{Bmatrix}_{6 \times 1} = \begin{bmatrix} [\tau_{PP}]_{2 \times 2} & [\tau_{PR}]_{2 \times 4} \\ [\tau_{RP}]_{4 \times 2} & [\tau_{RR}]_{4 \times 4} \end{bmatrix}_{6 \times 6} \begin{Bmatrix} \{\Delta x\}_{2 \times 1} \\ \{\Delta x_{Support}\}_{4 \times 1} \end{Bmatrix}_{6 \times 1}$$

$$\Rightarrow \{\Delta P\}_{2 \times 1} = [\tau_{PP}]_{2 \times 2} \{\Delta x\}_{2 \times 1} + [\tau_{PR}]_{2 \times 4} \{\Delta x_{Support}\}_{4 \times 1} \quad \Rightarrow \quad \{\Delta x\}_{2 \times 1}$$

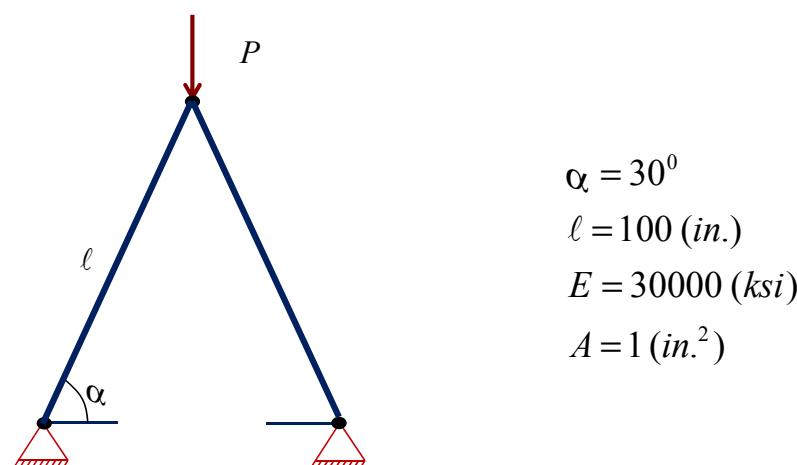
$$\Rightarrow \{\Delta R\}_{4 \times 1} = [\tau_{RP}]_{4 \times 2} \{\Delta x\}_{2 \times 1} + [\tau_{RR}]_{4 \times 4} \{\Delta x_{Support}\}_{4 \times 1} \quad \Rightarrow \quad \{\Delta R\}_{4 \times 1}$$

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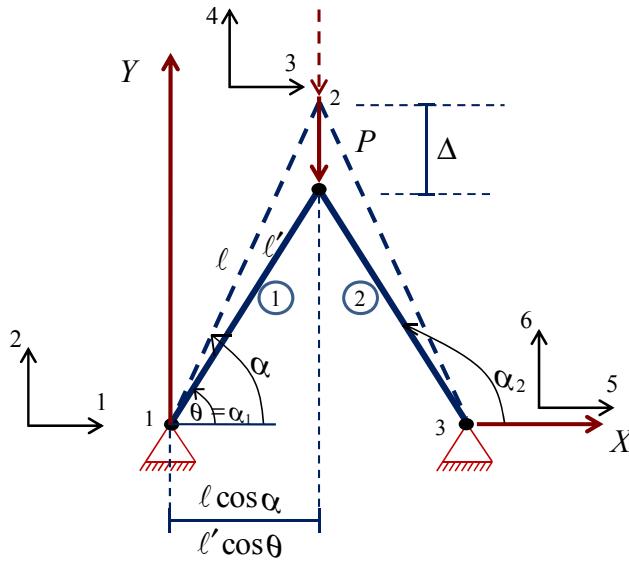
□ Example

مثال: در خریای نشان داده شده در شکل زیر مطلوب است تعیین الف) بار بحرانی و ب) جابجایی نقطه اثر بار $P=1500$ kips.



Geometrically Nonlinear Analysis of Plane Trusses

□ Example



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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$[T_1] = \begin{bmatrix} 1 & 2 & 3 & 4 & \\ \left(\frac{AE}{\ell}\right)_1 m_1^2 - \frac{Q_1}{\ell'_1} n_1^2 & \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'_1} m_1 n_1 & -\left(\frac{AE}{\ell}\right)_1 m_1^2 + \frac{Q_1}{\ell'_1} n_1^2 & -\left(\frac{AE}{\ell}\right)_1 m_1 n_1 - \frac{Q_1}{\ell'_1} m_1 n_1 & 1 \\ \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'_1} m_1 n_1 & \left(\frac{AE}{\ell}\right)_1 n_1^2 - \frac{Q_1}{\ell'_1} m_1^2 & -\left(\frac{AE}{\ell}\right)_1 m_1 n_1 - \frac{Q_1}{\ell'_1} m_1 n_1 & -\left(\frac{AE}{\ell}\right)_1 n_1^2 + \frac{Q_1}{\ell'_1} m_1^2 & 2 \\ -\left(\frac{AE}{\ell}\right)_1 m_1^2 + \frac{Q_1}{\ell'_1} n_1^2 & -\left(\frac{AE}{\ell}\right)_1 m_1 n_1 - \frac{Q_1}{\ell'_1} m_1 n_1 & \left(\frac{AE}{\ell}\right)_1 m_1^2 - \frac{Q_1}{\ell'_1} n_1^2 & \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'_1} m_1 n_1 & 3 \\ -\left(\frac{AE}{\ell}\right)_1 m_1 n_1 - \frac{Q_1}{\ell'_1} m_1 n_1 & -\left(\frac{AE}{\ell}\right)_1 n_1^2 + \frac{Q_1}{\ell'_1} m_1^2 & \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'_1} m_1 n_1 & \left(\frac{AE}{\ell}\right)_1 n_1^2 - \frac{Q_1}{\ell'_1} m_1^2 & 4 \end{bmatrix}$$

$$[T_2] = \left(\frac{AE}{\ell}\right)_2 [\bar{B}_2][\bar{B}_2]^T + Q_2 [g_2] = \left(\frac{AE}{\ell}\right)_2 \begin{bmatrix} m_2 \\ n_2 \\ -m_2 \\ -n_2 \end{bmatrix} \begin{bmatrix} m_2 \\ n_2 \\ -m_2 \\ -n_2 \end{bmatrix}^T + \frac{Q_2}{\ell'_2} \begin{bmatrix} -n_2^2 & m_2 n_2 & n_2^2 & -m_2 n_2 \\ m_2 n_2 & -m_2^2 & -m_2 n_2 & m_2^2 \\ n_2^2 & -m_2 n_2 & -n_2^2 & m_2 n_2 \\ -m_2 n_2 & m_2^2 & m_2 n_2 & -m_2^2 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$[T_2] = \begin{bmatrix} 3 & 4 & 5 & 6 & 3 \\ \left(\frac{AE}{\ell}\right)_2 m_2^2 - \frac{Q_2}{\ell'} n_2^2 & \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & -\left(\frac{AE}{\ell}\right)_2 m_2^2 + \frac{Q_2}{\ell'} n_2^2 & -\left(\frac{AE}{\ell}\right)_2 m_2 n_2 - \frac{Q_2}{\ell'} m_2 n_2 & 3 \\ \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & \left(\frac{AE}{\ell}\right)_2 n_2^2 - \frac{Q_2}{\ell'} m_2^2 & -\left(\frac{AE}{\ell}\right)_2 m_2 n_2 - \frac{Q_2}{\ell'} m_2 n_2 & -\left(\frac{AE}{\ell}\right)_2 n_2^2 + \frac{Q_2}{\ell'} m_2^2 & 4 \\ -\left(\frac{AE}{\ell}\right)_2 m_2^2 + \frac{Q_2}{\ell'} n_2^2 & -\left(\frac{AE}{\ell}\right)_2 m_2 n_2 - \frac{Q_2}{\ell'} m_2 n_2 & \left(\frac{AE}{\ell}\right)_2 m_2^2 - \frac{Q_2}{\ell'} n_2^2 & \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & 5 \\ -\left(\frac{AE}{\ell}\right)_2 m_2 n_2 - \frac{Q_2}{\ell'} m_2 n_2 & -\left(\frac{AE}{\ell}\right)_2 n_2^2 + \frac{Q_2}{\ell'} m_2^2 & \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & \left(\frac{AE}{\ell}\right)_2 n_2^2 - \frac{Q_2}{\ell'} m_2^2 & 6 \end{bmatrix}$$

$$[\tau] = \begin{bmatrix} 1 & 2 & 3 & 4 & 5 & 6 & 7 \\ T_{11}^{(1)} & T_{12}^{(1)} & T_{13}^{(1)} & T_{14}^{(1)} & 0 & 0 & 1 \\ T_{21}^{(1)} & T_{22}^{(1)} & T_{23}^{(1)} & T_{24}^{(1)} & 0 & 0 & 2 \\ T_{31}^{(1)} & T_{32}^{(1)} & T_{33}^{(1)} + T_{33}^{(2)} & T_{34}^{(1)} + T_{34}^{(2)} & T_{35}^{(2)} & T_{36}^{(2)} & 3 \\ T_{41}^{(1)} & T_{42}^{(1)} & T_{43}^{(1)} + T_{43}^{(2)} & T_{44}^{(1)} + T_{44}^{(2)} & T_{45}^{(2)} & T_{45}^{(2)} & 4 \\ 0 & 0 & T_{53}^{(2)} & T_{54}^{(2)} & T_{55}^{(2)} & T_{55}^{(2)} & 5 \\ 0 & 0 & T_{63}^{(2)} & T_{64}^{(2)} & T_{65}^{(2)} & T_{65}^{(2)} & 6 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$[\tau_{PP}]_{2 \times 2} = \begin{bmatrix} 3 & 4 & 3 \\ \left(\frac{AE}{\ell}\right)_1 m_1^2 - \frac{Q_1}{\ell'} n_1^2 + \left(\frac{AE}{\ell}\right)_2 m_2^2 - \frac{Q_2}{\ell'} n_2^2 & \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'} m_1 n_1 + \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & 3 \\ \left(\frac{AE}{\ell}\right)_1 m_1 n_1 + \frac{Q_1}{\ell'} m_1 n_1 + \left(\frac{AE}{\ell}\right)_2 m_2 n_2 + \frac{Q_2}{\ell'} m_2 n_2 & \left(\frac{AE}{\ell}\right)_1 n_1^2 - \frac{Q_1}{\ell'} m_1^2 + \left(\frac{AE}{\ell}\right)_2 n_2^2 - \frac{Q_2}{\ell'} m_2^2 & 4 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$\left(\frac{AE}{\ell} \right)_1 = \left(\frac{AE}{\ell} \right)_2 = \frac{AE}{\ell} \quad \& \quad \frac{Q_1}{\ell'_1} = \frac{Q_2}{\ell'_2} = \frac{Q}{\ell'} \Rightarrow$$

$$[\mathbf{t}_{PP}]_{2 \times 2} = \frac{AE}{\ell} \begin{bmatrix} 3 & 4 & 3 \\ m_1^2 + m_2^2 & m_1 n_1 + m_2 n_2 & 3 \\ m_1 n_1 + m_2 n_2 & n_1^2 + n_2^2 & 4 \end{bmatrix} + \frac{Q}{\ell'} \begin{bmatrix} 3 & 4 & 3 \\ -n_1^2 - n_2^2 & m_1 n_1 + m_2 n_2 & 3 \\ m_1 n_1 + m_2 n_2 & -m_1^2 - m_2^2 & 4 \end{bmatrix}$$

$$\begin{aligned} m &= m_1 = -m_2 = \cos \theta \\ n &= n_1 = n_2 = \sin \theta \end{aligned}$$

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{AE}{\ell} \begin{bmatrix} 2m^2 & 0 \\ 0 & 2n^2 \end{bmatrix} + \frac{Q}{\ell'} \begin{bmatrix} -2n^2 & 0 \\ 0 & -2m^2 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell \cos \alpha} \begin{bmatrix} \cos \alpha - \sin^2 \theta \cos \theta & 0 \\ 0 & \cos \alpha - \cos^3 \theta \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

خرپا چه زمانی ناپایدار می‌شود؟

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Geometrically Nonlinear Analysis of Plane Trusses

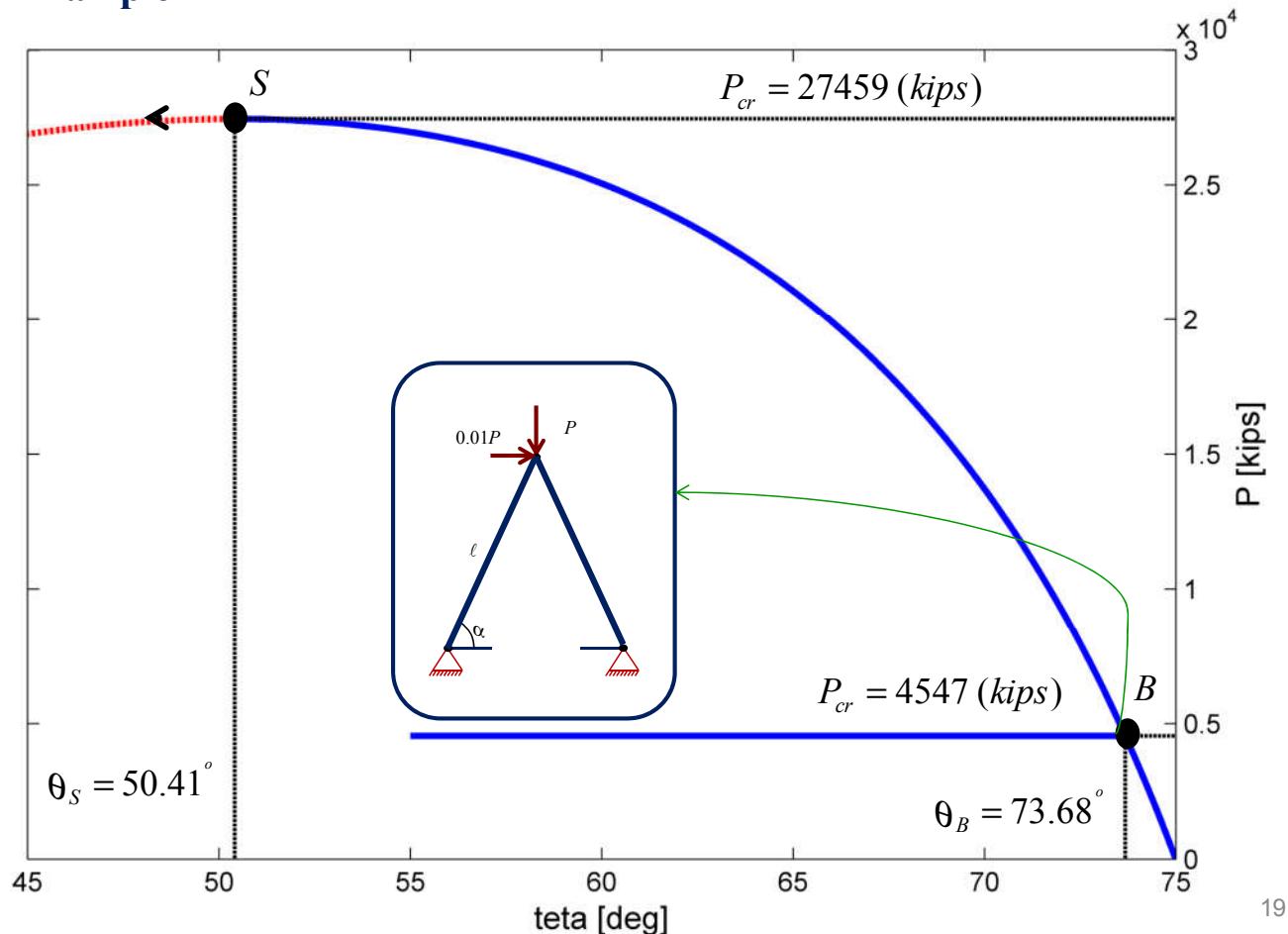
□ Example

در چه حالتی مودهای ناپایداری Snap through و Bifurcation همزمان اتفاق می‌افتد.

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Geometrically Nonlinear Analysis of Plane Trusses

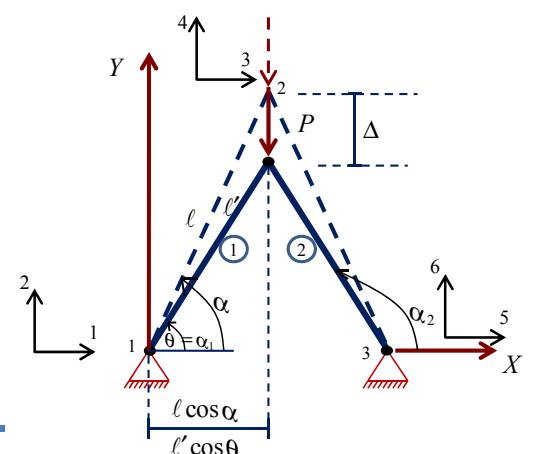
□ Example



Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$\Rightarrow \ell'_1 = \ell \left[1 - 2 \frac{\Delta}{\ell} \sin \alpha + \left(\frac{\Delta}{\ell} \right)^2 \right]^{\frac{1}{2}}$$



$$\Rightarrow \ell'_2 = \ell'_1 = \ell' = \ell \left[1 - 2 \frac{\Delta}{\ell} \sin \alpha + \left(\frac{\Delta}{\ell} \right)^2 \right]^{\frac{1}{2}}$$

Geometrically Nonlinear Analysis of Plane Trusses

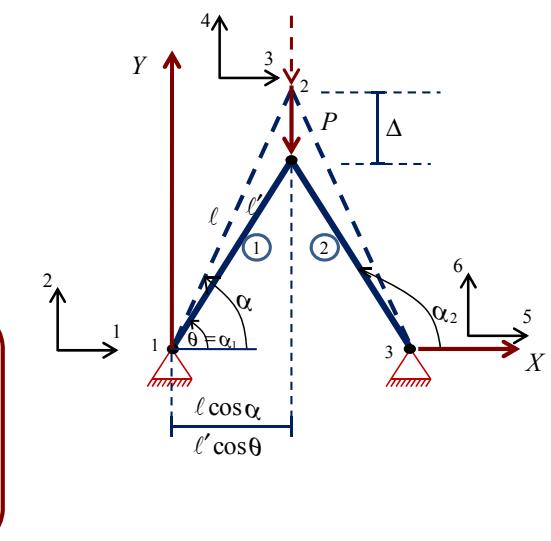
□ Example

$$m_1 = \frac{\ell \cos \alpha}{\ell'}$$

$$n_1 = \frac{\ell \sin \alpha - \Delta}{\ell'}$$

$$m_2 = -\frac{\ell \cos \alpha}{\ell'}$$

$$n_2 = \frac{\ell \sin \alpha - \Delta}{\ell'}$$



$$\Rightarrow [k_{PP}] = \frac{AE}{\ell} \begin{bmatrix} 2m^2 & 0 \\ 0 & 2n^2 \end{bmatrix} + \frac{Q}{\ell'} \begin{bmatrix} -2n^2 & 0 \\ 0 & -2m^2 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

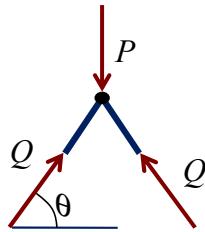
□ Example

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

در هر مرحله باید تعادل گره‌ای بررسی شود برای این منظور باید تعادل را در دو راستای 3 و 4 کنترل کرد. اما چون در راستای 3 نیرویی وارد نمی‌شود نیازی به کنترل تعادل در این راستا نیست.



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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

یادآوری

$$[\mathbf{t}_{PP}] = \frac{AE}{\ell} \begin{bmatrix} 2m^2 & 0 \\ 0 & 2n^2 \end{bmatrix} + \frac{Q}{\ell'} \begin{bmatrix} -2n^2 & 0 \\ 0 & -2m^2 \end{bmatrix}$$
$$\Rightarrow [\mathbf{t}_{PP}] = \frac{AE}{\ell} \begin{bmatrix} 2\left(\frac{\ell \cos \alpha}{\ell \beta}\right)^2 & 0 \\ 0 & 2\left(\frac{\ell \sin \alpha - \Delta}{\ell \beta}\right)^2 \end{bmatrix} + \frac{AE}{\ell} \left(\frac{1-\beta}{\beta} \right) \begin{bmatrix} -2\left(\frac{\ell \sin \alpha - \Delta}{\ell \beta}\right)^2 & 0 \\ 0 & -2\left(\frac{\ell \cos \alpha}{\ell \beta}\right)^2 \end{bmatrix}$$
$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell} \begin{bmatrix} \left(\frac{\ell \cos \alpha}{\ell \beta}\right)^2 - \left(\frac{1-\beta}{\beta}\right) \left(\frac{\sin \alpha - \frac{\Delta}{\ell}}{\beta}\right)^2 & 0 \\ 0 & \left(\frac{\sin \alpha - \frac{\Delta}{\ell}}{\beta}\right)^2 - \left(\frac{1-\beta}{\beta}\right) \left(\frac{\ell \cos \alpha}{\ell \beta}\right)^2 \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell\beta^2} \begin{bmatrix} \cos^2 \alpha - \left(\frac{1}{\beta} - 1\right) \left(\sin \alpha - \frac{\Delta}{\ell}\right)^2 & 0 \\ 0 & \left(\sin \alpha - \frac{\Delta}{\ell}\right)^2 - \left(\frac{1}{\beta} - 1\right) \cos^2 \alpha \end{bmatrix}$$

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell\beta^2} \begin{bmatrix} \cos^2 \alpha - \frac{\left(\sin \alpha - \frac{\Delta}{\ell}\right)^2}{\beta} + \left(\sin \alpha - \frac{\Delta}{\ell}\right)^2 & 0 \\ 0 & \left(\sin \alpha - \frac{\Delta}{\ell}\right)^2 - \frac{\cos^2 \alpha}{\beta} + \cos^2 \alpha \end{bmatrix}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell\beta^2} \begin{bmatrix} \cos^2 \alpha - \frac{\beta^2 - \cos^2 \alpha}{\beta} + \beta^2 - \cos^2 \alpha & 0 \\ 0 & \beta^2 - \cos^2 \alpha - \frac{\cos^2 \alpha}{\beta} + \cos^2 \alpha \end{bmatrix}$$

$$\Rightarrow [\mathbf{t}_{PP}] = \frac{2AE}{\ell} \begin{bmatrix} 1 - \frac{\beta^2 - \cos^2 \alpha}{\beta^3} & 0 \\ 0 & 1 - \frac{\cos^2 \alpha}{\beta^3} \end{bmatrix} \quad (II)$$

$$\beta = \left[1 - 2 \frac{\Delta}{\ell} \sin \alpha + \left(\frac{\Delta}{\ell} \right)^2 \right]^{\frac{1}{2}}$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

خرپا چه زمانی ناپایدار می شود؟

با استفاده از روش Linear Incremental Method with Iteration

Updated Newton Raphson Iteration (Updated N.R.It)

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

(2)

$$\{\mathbf{x}^{(2)}\} = \{\mathbf{x}^{(1)}\} + \{\Delta\mathbf{x}^{(1)}\} = \begin{Bmatrix} 0 \\ 10 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 4.18 \end{Bmatrix} \Rightarrow \{\mathbf{x}^{(2)}\} = \begin{Bmatrix} 0 \\ 14.18 \end{Bmatrix} (\text{in}) \xrightarrow{(I)} \{\mathbf{P}_{\mathbf{x}^{(2)}}\} = \begin{Bmatrix} 0 \\ 1440.6 \end{Bmatrix} (\text{kips})$$

$$\{\Delta\mathbf{Q}^{(2)}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \{\mathbf{P}_{\mathbf{x}^{(2)}}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \begin{Bmatrix} 0 \\ 1440.6 \end{Bmatrix} \Rightarrow \{\Delta\mathbf{Q}^{(2)}\} = \begin{Bmatrix} 0 \\ 59.384 \end{Bmatrix} (\text{kips})$$

$$(II) \Rightarrow [\boldsymbol{\tau}_{\mathbf{x}^{(2)}}] = \begin{bmatrix} 506.47 & 0 \\ 0 & 53.308 \end{bmatrix} (\text{kips/in})$$

$$\stackrel{(\text{Equation 2-22})}{\Rightarrow} \{\Delta\mathbf{x}^{(2)}\} = [\boldsymbol{\tau}^{(2)}]^{-1} \{\Delta\mathbf{Q}^{(2)}\} \Rightarrow \{\Delta\mathbf{x}^{(2)}\} = \begin{Bmatrix} 0 \\ 1.114 \end{Bmatrix} (\text{in.})$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

(3)

$$\{\mathbf{x}^{(3)}\} = \{\mathbf{x}^{(2)}\} + \{\Delta\mathbf{x}^{(2)}\} = \begin{Bmatrix} 0 \\ 14.18 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 1.114 \end{Bmatrix} \Rightarrow \{\mathbf{x}^{(3)}\} = \begin{Bmatrix} 0 \\ 15.294 \end{Bmatrix} (\text{in}) \xrightarrow{(I)} \{\mathbf{P}_{\mathbf{x}^{(3)}}\} = \begin{Bmatrix} 0 \\ 1495.9 \end{Bmatrix} (\text{kips})$$

$$\{\Delta\mathbf{Q}^{(3)}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \{\mathbf{P}_{\mathbf{x}^{(3)}}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \begin{Bmatrix} 0 \\ 1495.9 \end{Bmatrix} \Rightarrow \{\Delta\mathbf{Q}^{(3)}\} = \begin{Bmatrix} 0 \\ 4.1372 \end{Bmatrix} (\text{kips})$$

$$(II) \Rightarrow [\boldsymbol{\tau}_{\mathbf{x}^{(3)}}] = \begin{bmatrix} 511.01 & 0 \\ 0 & 45.89 \end{bmatrix} (\text{kips/in})$$

$$\stackrel{(\text{Equation 2-22})}{\Rightarrow} \{\Delta\mathbf{x}^{(3)}\} = [\boldsymbol{\tau}^{(3)}]^{-1} \{\Delta\mathbf{Q}^{(3)}\} \Rightarrow \{\Delta\mathbf{x}^{(3)}\} = \begin{Bmatrix} 0 \\ 0.090156 \end{Bmatrix} (\text{in.})$$

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example

(4)

$$\{\mathbf{x}^{(4)}\} = \{\mathbf{x}^{(3)}\} + \{\Delta\mathbf{x}^{(3)}\} = \begin{Bmatrix} 0 \\ 15.294 \end{Bmatrix} + \begin{Bmatrix} 0 \\ 0.0902 \end{Bmatrix} \Rightarrow \boxed{\{\mathbf{x}^{(4)}\} = \begin{Bmatrix} 0 \\ 15.38416 \end{Bmatrix} (\text{in})} \xrightarrow{(I)} \boxed{\{\mathbf{P}_{\mathbf{x}^{(4)}}^{(4)}\} = \begin{Bmatrix} 0 \\ 1499.97 \end{Bmatrix} (\text{kips})}$$

$$\{\Delta\mathbf{Q}^{(4)}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \{\mathbf{P}_{\mathbf{x}^{(4)}}^{(4)}\} = \begin{Bmatrix} 0 \\ 1500 \end{Bmatrix} - \begin{Bmatrix} 0 \\ 1499.97 \end{Bmatrix} \Rightarrow \boxed{\{\Delta\mathbf{Q}^{(4)}\} = \begin{Bmatrix} 0 \\ 0.0269 \end{Bmatrix} (\text{kips})}$$

$$(II) \Rightarrow \boxed{[\tau_{\mathbf{x}^{(4)}}^{(4)}] = \begin{bmatrix} 511.38 & 0 \\ 0 & 45.287 \end{bmatrix} (\text{kips/in})}$$

$$\xrightarrow{\text{(Equation 2-22)}} \{\Delta\mathbf{x}^{(4)}\} = [\tau^{(4)}]^{-1} \{\Delta\mathbf{Q}^{(4)}\} \Rightarrow \boxed{\{\Delta\mathbf{x}^{(4)}\} = \begin{Bmatrix} 0 \\ 0.0006 \end{Bmatrix} (\text{in.})}$$

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Geometrically Nonlinear Analysis of Plane Trusses

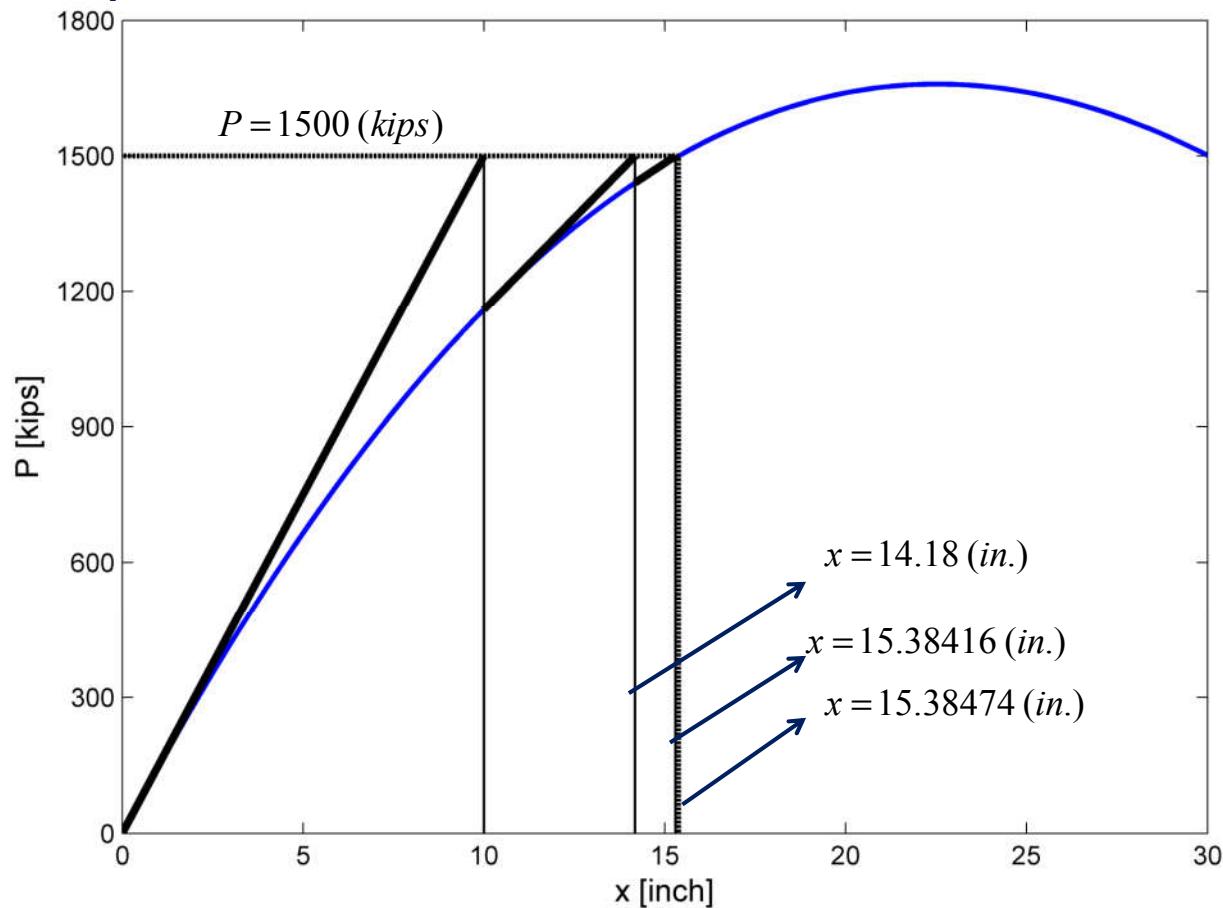
□ Example

| Iteration | $P^{(i)}$ (kips) | $x^{(i)}$ (in.) | $\tau^{(i)}$ (kips/in.) | $\Delta Q^{(i)}$ (kips) | $\Delta x^{(i)}$ (in.) | $x^{(i+1)}$ (in.) |
|-----------|------------------|-----------------|-------------------------|-------------------------|------------------------|-------------------|
| 0 | 0 | 0 | 150.000 | 1500 | 10 | 10 |
| 1 | 1158.836 | 10 | 81.617 | 341.1639 | 4.1800 | 14.18004 |
| 2 | 1440.618 | 14.18004 | 53.308 | 59.38181 | 1.1139 | 15.29399 |
| 3 | 1495.862 | 15.29399 | 45.890 | 4.137854 | 0.0902 | 15.38416 |
| 4 | 1499.973 | 15.38416 | 45.292 | 0.026937 | 0.0006 | 15.38475 |
| 5 | 1500 | 15.38475 | 45.288 | 1.17E-06 | 0.0000 | 15.38475 |

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Geometrically Nonlinear Analysis of Plane Trusses

□ Example



Updated Newton Raphson Iteration (Updated N.R.It)