



دانشگاه کردستان  
University of Kurdistan  
زانکۆی کوردستان

# Mechanics of Materials

Ferdinand P.Beer, E.Russel Johnston, Jr., John T.Dewolf

Other Reference:

J.Wat Oler "Lectures notes on Mechanics of Materials"

Ibrahim A.Assakkaf "Lectures notes on Mechanics of Materials"

## Energy Methods

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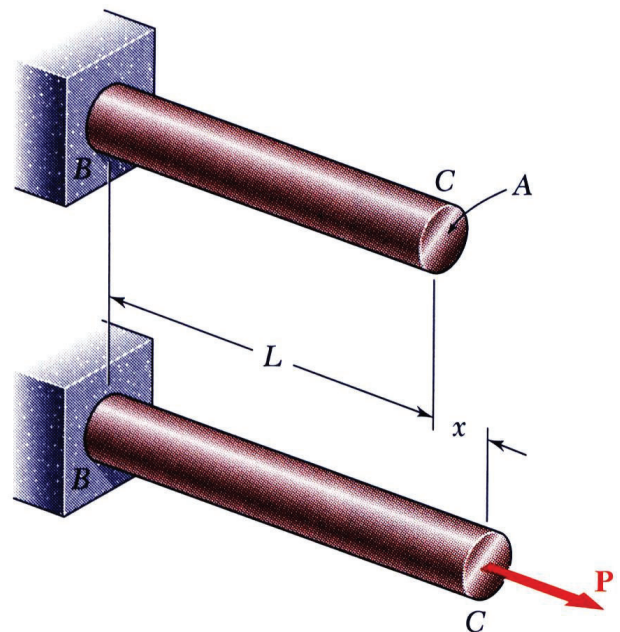
<https://prof.uok.ac.ir/Ka.Karami>

### Energy Methods

#### □ Strain Energy

- A uniform rod is subjected to a slowly increasing load
- The **elementary work** done by the load  $P$  as the rod elongates by a small  $dx$  is

$$dU = P dx = \text{elementary work}$$

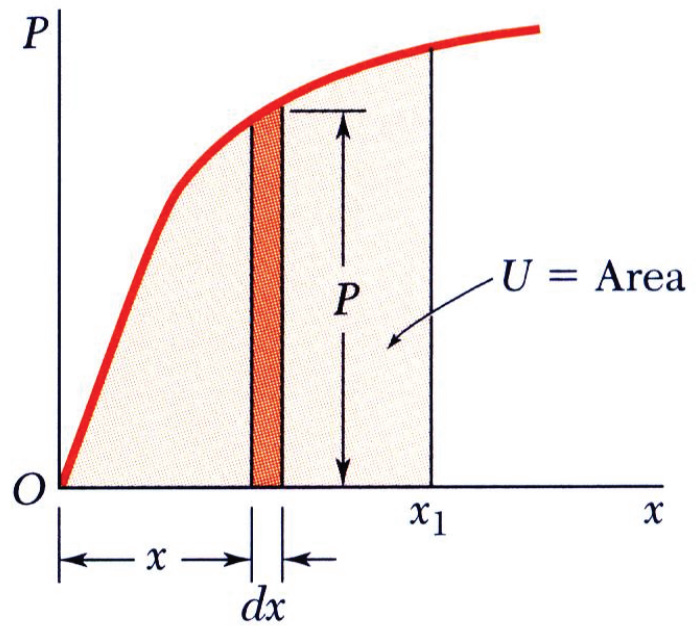


## Energy Methods

### □ Strain Energy

$$dU = P dx = \text{elementary work}$$

which is equal to the area of width  $dx$  under the load-deformation diagram.



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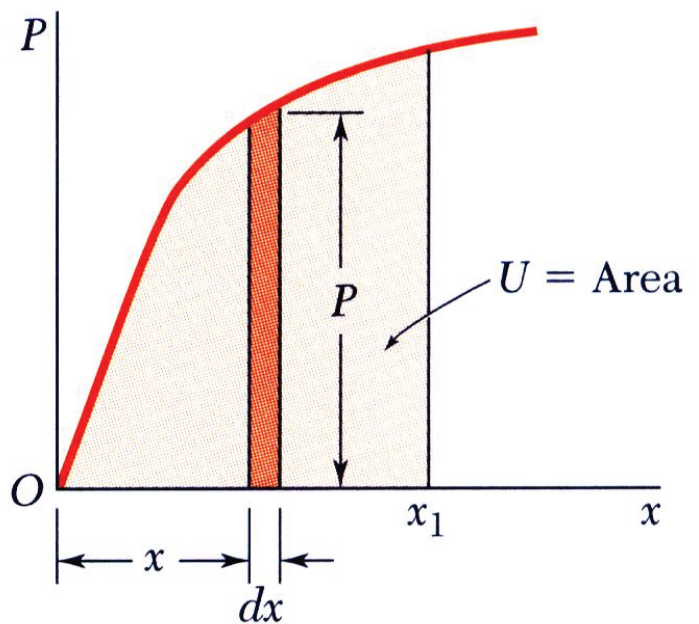
## Energy Methods

### □ Strain Energy

- The *total work* done by the load for a deformation  $x_1$ ,

$$U = \int_0^{x_1} P dx = \text{total work} = \text{strain energy}$$

which results in an increase of *strain energy* in the rod.



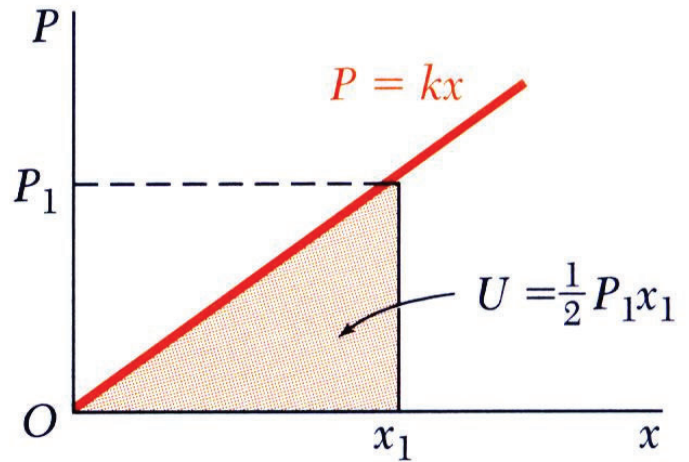
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## Energy Methods

### □ Strain Energy

- In the case of a linear elastic deformation,

$$U = \int_0^{x_1} kx \, dx = \frac{1}{2} kx_1^2 = \frac{1}{2} P_1 x_1$$



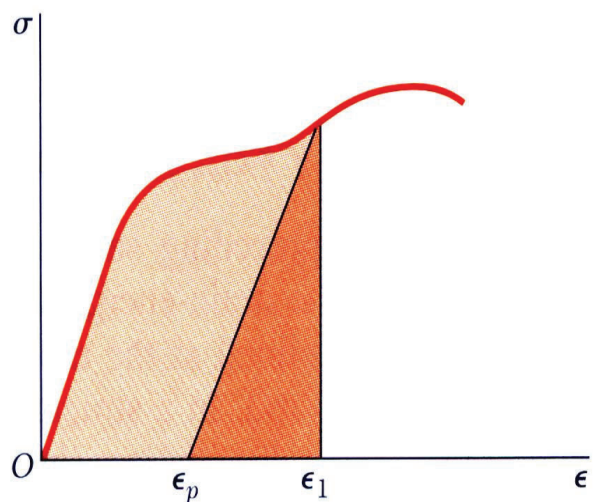
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## Energy Methods

### □ Strain Energy Density

- To eliminate the effects of size, evaluate the strain- energy per unit volume,
- The total strain energy density resulting from the deformation is equal to the area under the curve to  $\epsilon_1$ .
- As the material is unloaded, the stress returns to zero but there is a permanent deformation. Only the strain energy represented by the triangular area is recovered.
- Remainder of the energy spent in deforming the material is dissipated as heat.

$$\frac{U}{V} = \int_0^{\epsilon_1} \frac{P}{A} \frac{dx}{L}$$
$$u = \int_0^{\epsilon_1} \sigma_x \, d\epsilon = \text{strain energy density}$$

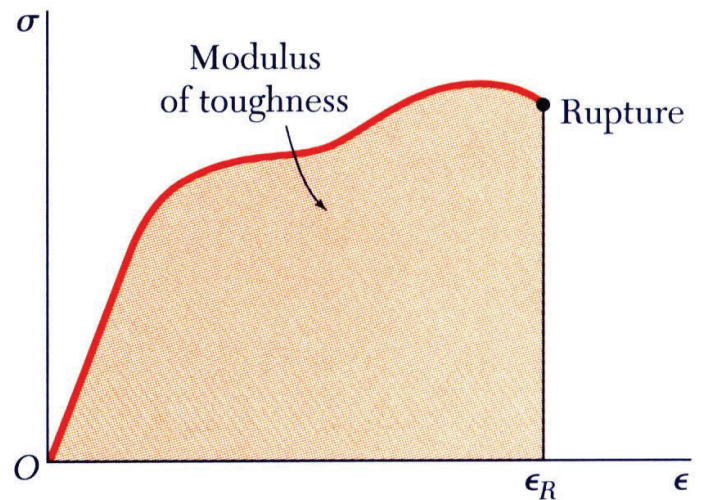


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## Energy Methods

### □ Strain Energy Density

- The strain energy density resulting from setting  $\epsilon_1 = \epsilon_R$  is the *modulus of toughness*.
- The energy per unit volume required to cause the material to rupture is related to its ductility as well as its ultimate strength.



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## Energy Methods

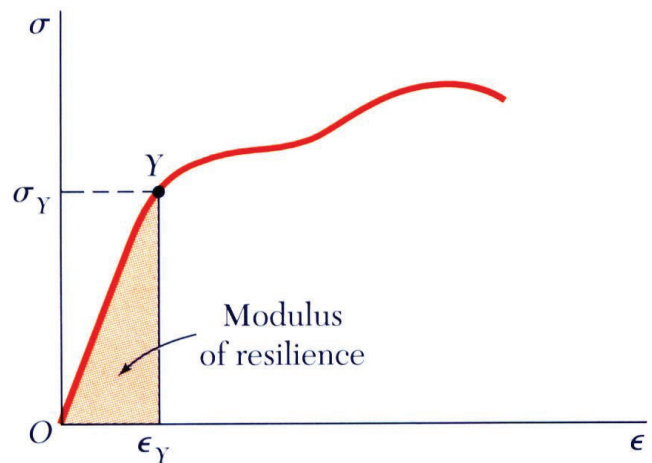
### □ Strain Energy Density

- If the stress remains within the proportional limit,

$$u = \int E \epsilon_x d\epsilon_x = \frac{E \epsilon_x^2}{2} = \frac{\sigma_x^2}{2E}$$

- The strain energy density resulting from setting  $\sigma_1 = \sigma_Y$  is the *modulus of resilience*.

$$u_Y = \frac{\sigma_Y^2}{2E} = \text{modulus of resilience}$$



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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

- In an element with a Nonuniform stress distribution,

$$u = \lim_{\Delta V \rightarrow 0} \frac{\Delta U}{\Delta V} = \frac{dU}{dV} \quad U = \int u \, dV = \text{total strain energy}$$

- For values of  $u < u_Y$ , i.e., below the proportional limit,

$$U = \int \frac{\sigma_x^2}{2E} dV = \text{elastic strain energy}$$

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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

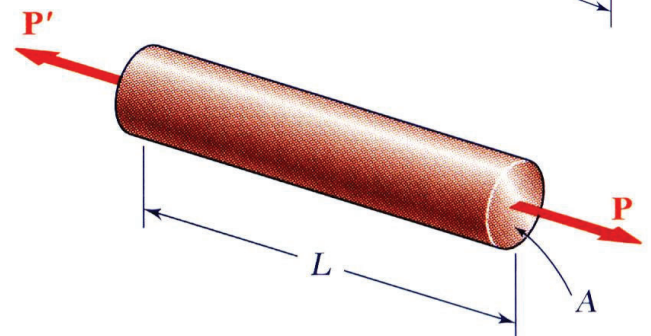
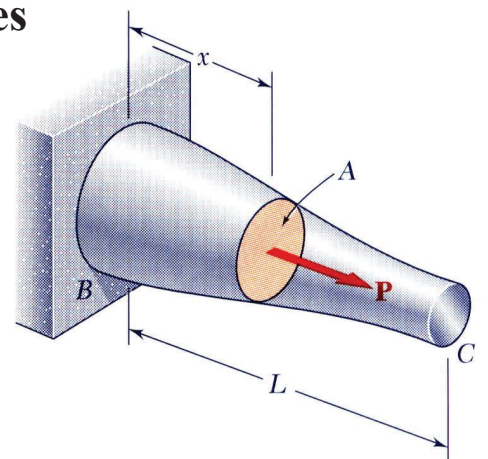
- Under axial loading,

$$\sigma_x = P/A \quad dV = A \, dx \quad \Rightarrow$$

$$U = \int_0^L \frac{P^2}{2AE} dx$$

- For a rod of uniform cross-section,

$$U = \frac{P^2 L}{2AE}$$



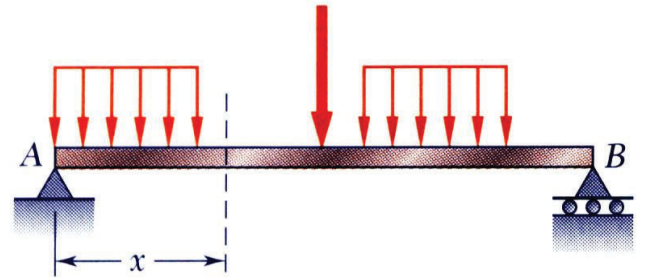
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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

- For a beam subjected to a bending load,

$$\sigma_x = \frac{M y}{I} \Rightarrow U = \int \frac{\sigma_x^2}{2E} dV = \int \frac{M^2 y^2}{2EI^2} dV$$



- Setting  $dV = dA dx$ ,

$$U = \int_0^L \int_A \frac{M^2 y^2}{2EI^2} dA dx = \int_0^L \frac{M^2}{2EI^2} \left( \int_A y^2 dA \right) dx \Rightarrow U = \int_0^L \frac{M^2}{2EI} dx$$

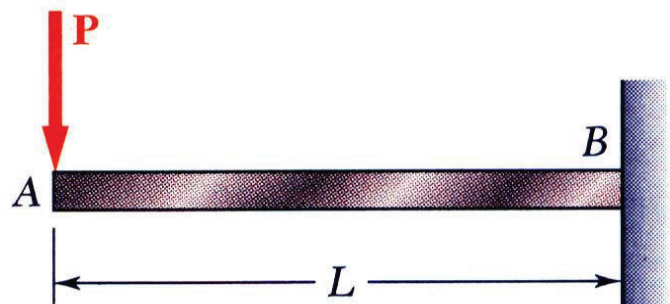
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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 01

- Determine the total strain energy due to exerted force on the cantilever beam.



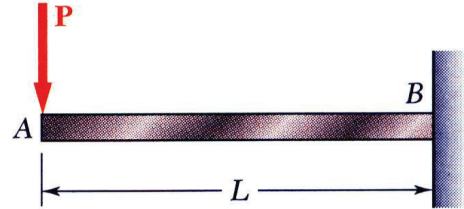
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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 01

- For an end-loaded cantilever beam,



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## Energy Methods

### □ Strain Energy For Shearing Stresses

- For a material subjected to plane shearing stresses,

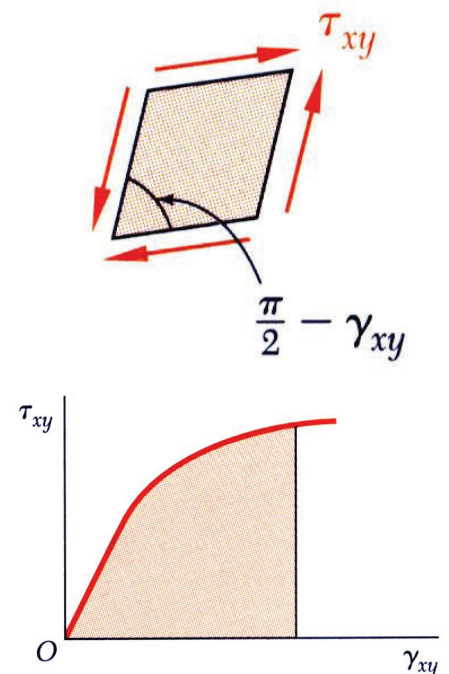
$$u = \int_0^{\gamma_{xy}} \tau_{xy} d\gamma_{xy}$$

- For values of  $\tau_{xy}$  within the proportional limit,

$$u = \frac{1}{2} G \gamma_{xy}^2 = \frac{1}{2} \tau_{xy} \gamma_{xy} = \frac{\tau_{xy}^2}{2G}$$

- The total strain energy is found from

$$U = \int u dV \Rightarrow U = \int \frac{\tau_{xy}^2}{2G} dV$$



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## Energy Methods

### □ Strain Energy For Shearing Stresses

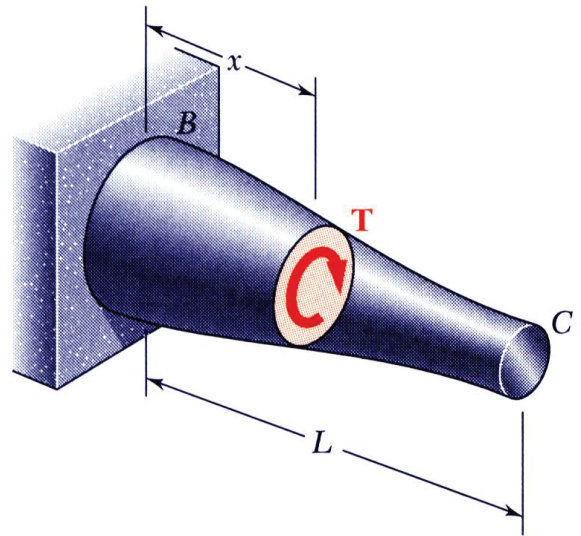
- For a shaft subjected to a torsional load,

$$\tau_{xy} = \frac{T\rho}{J} \Rightarrow U = \int \frac{\tau_{xy}^2}{2G} dV = \int \frac{T^2 \rho^2}{2GJ^2} dV$$

- Setting  $dV = dA dx$ ,

$$U = \int_0^L \int_A \frac{T^2 \rho^2}{2GJ^2} dA dx = \int_0^L \frac{T^2}{2GJ^2} \left( \int_A \rho^2 dA \right) dx$$

$$\Rightarrow U = \int_0^L \frac{T^2}{2GJ} dx$$



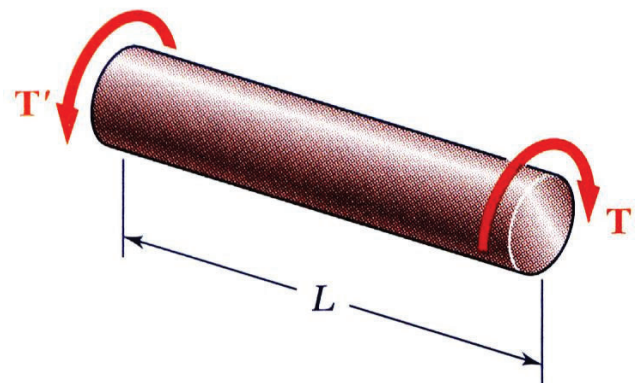
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## Energy Methods

### □ Strain Energy For Shearing Stresses

- In the case of a uniform shaft,

$$U = \int_0^L \frac{T^2}{2GJ} dx \Rightarrow U = \frac{T^2 L}{2GJ}$$



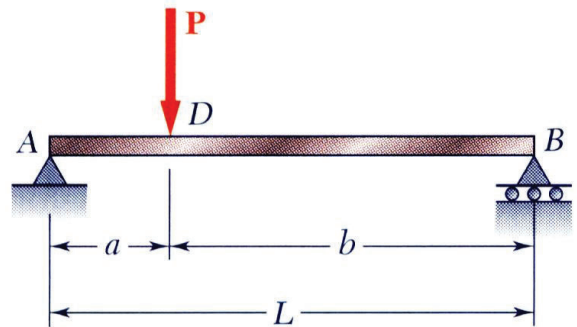
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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 02

- Taking into account only the normal stresses due to bending, determine the strain energy of the beam for the loading shown.
- Evaluate the strain energy knowing that the beam is a W10x45,  $P = 40$  kips,  $L = 12$  ft,  $a = 3$  ft,  $b = 9$  ft, and  $E = 29 \times 10^6$  psi.

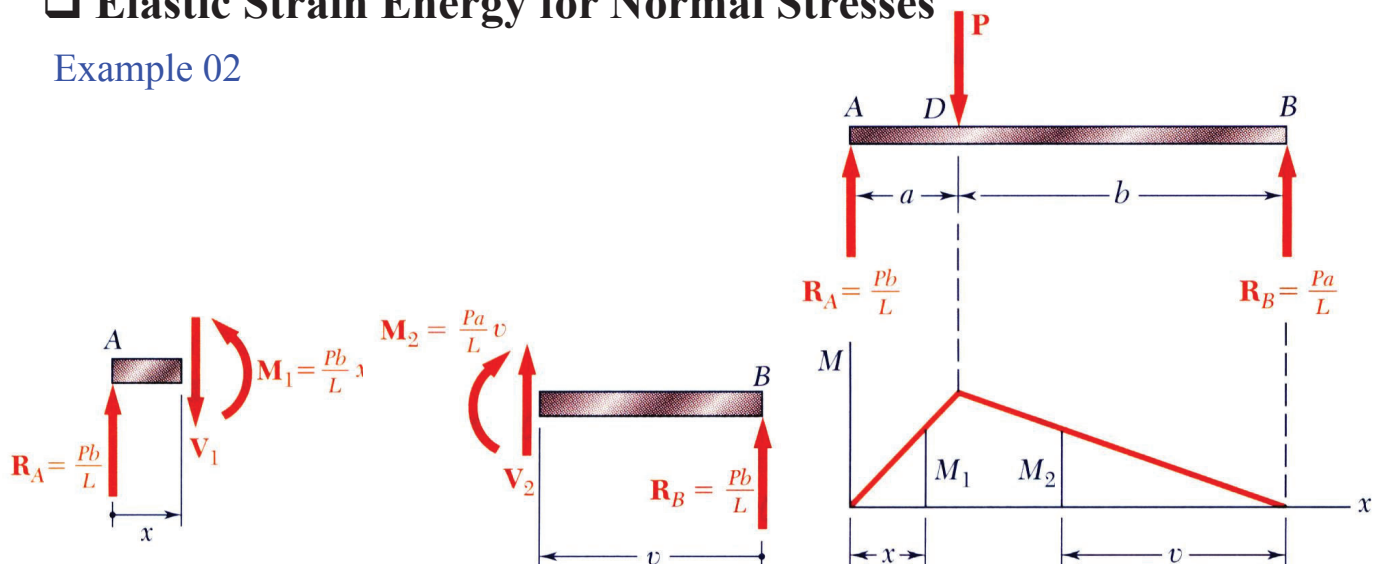


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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 02



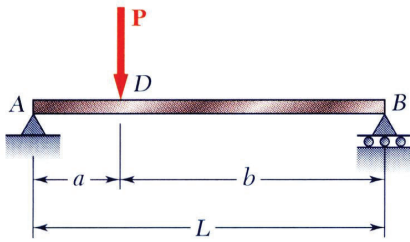
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## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 02

- Integrate over the volume of the beam to find the strain energy.



Over the portion AD,

$$M_1 = \frac{Pb}{L}x$$

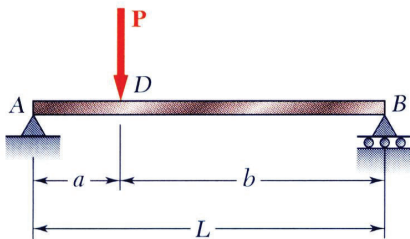
Over the portion BD,

$$M_2 = \frac{Pa}{L}v$$

## Energy Methods

### □ Elastic Strain Energy for Normal Stresses

#### Example 02



$$\begin{aligned} P &= 45 \text{ kips} & L &= 144 \text{ in.} \\ a &= 36 \text{ in.} & b &= 108 \text{ in.} \\ E &= 29 \times 10^3 \text{ ksi} & I &= 248 \text{ in}^4 \end{aligned}$$

## Energy Methods

### □ Strain Energy for a General State of Stress

- Previously found strain energy due to uniaxial stress and plane shearing stress. For a general state of stress,

$$u = \frac{1}{2}(\sigma_x \epsilon_x + \sigma_y \epsilon_y + \sigma_z \epsilon_z + \tau_{xy} \gamma_{xy} + \tau_{yz} \gamma_{yz} + \tau_{zx} \gamma_{zx})$$

- With respect to the principal axes for an elastic, isotropic body,

$$u = \frac{1}{2E}[\sigma_a^2 + \sigma_b^2 + \sigma_c^2 - 2\nu(\sigma_a \sigma_b + \sigma_b \sigma_c + \sigma_c \sigma_a)] = u_v + u_d$$

$$u_v = \frac{1-2\nu}{6E}(\sigma_a + \sigma_b + \sigma_c)^2 = \text{due to volume change}$$

$$u_d = \frac{1}{12G}[(\sigma_a - \sigma_b)^2 + (\sigma_b - \sigma_c)^2 + (\sigma_c - \sigma_a)^2] = \text{due to distortion}$$

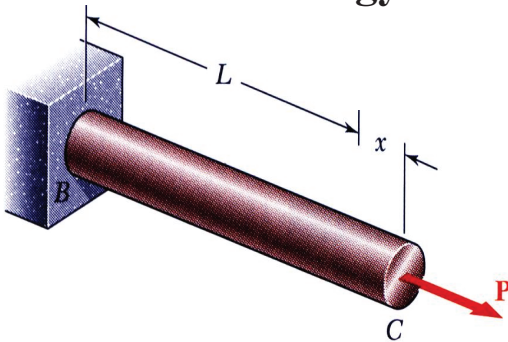
- Basis for the *maximum distortion energy* failure criteria,

$$u_d < (u_d)_Y = \frac{\sigma_Y^2}{6G} \text{ for a tensile test specimen}$$

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## Energy Methods

### □ Work and Energy Under a Single Load



- Previously, we found the strain energy by integrating the energy density over the volume.

For a uniform rod,

$$\begin{aligned} U &= \int u dV = \int \frac{\sigma^2}{2E} dV \\ &= \int_0^L \frac{(P_1/A)^2}{2E} A dx = \frac{P_1^2 L}{2AE} \end{aligned}$$

- Strain energy may also be found from the work of the single load  $P_1$ ,

$$U = \int_0^{x_1} P dx$$

- For an elastic deformation,

$$U = \int_0^{x_1} P dx = \int_0^{x_1} kx dx = \frac{1}{2} kx_1^2 = \frac{1}{2} P_1 x_1$$

- Knowing the relationship between force and displacement,

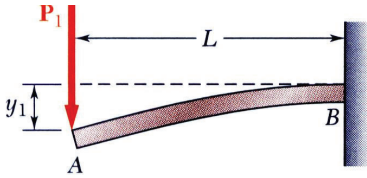
$$x_1 = \frac{P_1 L}{AE} \Rightarrow U = \frac{1}{2} P_1 \left( \frac{P_1 L}{AE} \right) = \frac{P_1^2 L}{2AE}$$

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## Energy Methods

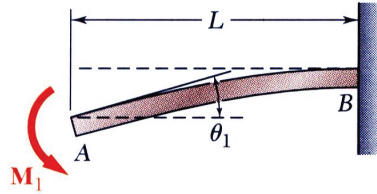
### □ Work and Energy Under a Single Load

- Transverse load



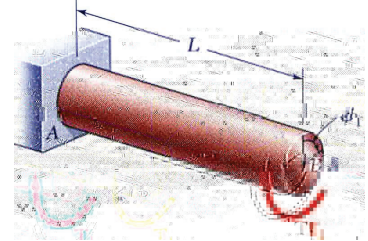
$$U = \int_0^{y_1} P dy = \frac{1}{2} P_1 y_1$$
$$= \frac{1}{2} P_1 \left( \frac{P_1 L^3}{3EI} \right) = \frac{P_1^2 L^3}{6EI}$$

- Bending couple



$$U = \int_0^{\theta_1} M d\theta = \frac{1}{2} M_1 \theta_1$$
$$= \frac{1}{2} M_1 \left( \frac{M_1 L}{EI} \right) = \frac{M_1^2 L}{2EI}$$

- Torsional couple



$$U = \int_0^{\phi_1} T d\phi = \frac{1}{2} T_1 \phi_1$$
$$= \frac{1}{2} T_1 \left( \frac{T_1 L}{JG} \right) = \frac{T_1^2 L}{2JG}$$

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## Energy Methods

### □ Deflection Under a Single Load

- If the strain energy of a structure due to a single concentrated load is known, then the equality between the work of the load and energy may be used to find the deflection.

***Work = Energy  $\Rightarrow$***

***Deflection***

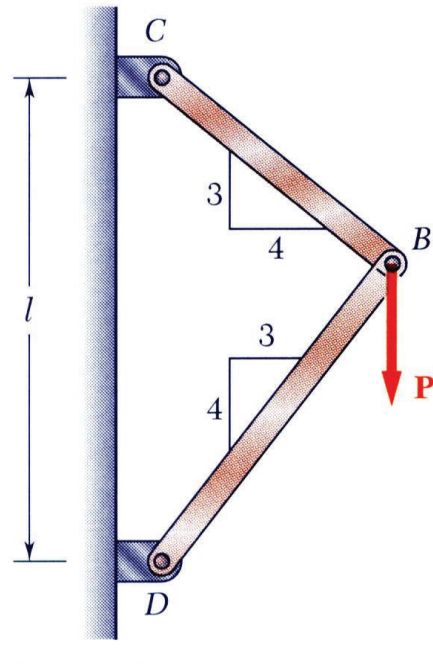
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 03

Determine vertical deflection at point B.



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## Energy Methods

### □ Deflection Under a Single Load

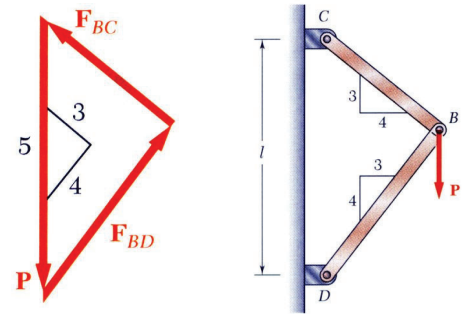
#### Example 03

From the given geometry,

- Strain energy of the structure,

From statics,

- Equating work and strain energy,



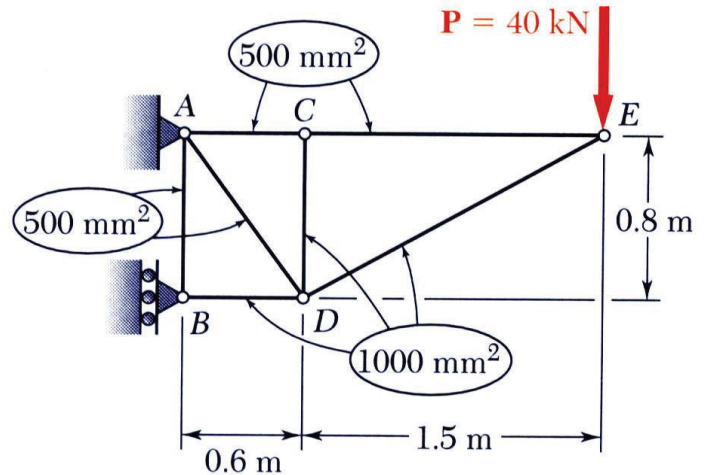
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 04

Members of the truss shown consist of sections of aluminum pipe with the cross-sectional areas indicated. Using  $E = 73 \text{ GPa}$ , determine the vertical deflection of the point  $E$  caused by the load  $P$ .



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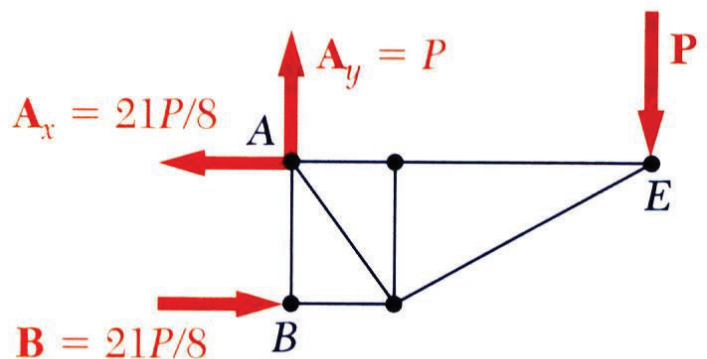
## Energy Methods

### □ Deflection Under a Single Load

#### Example 04

SOLUTION:

- Find the reactions at A and B from a free-body diagram of the entire truss.



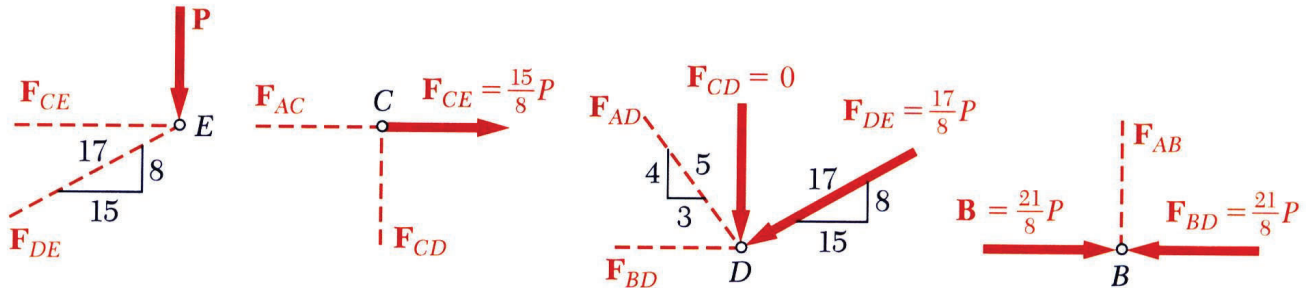
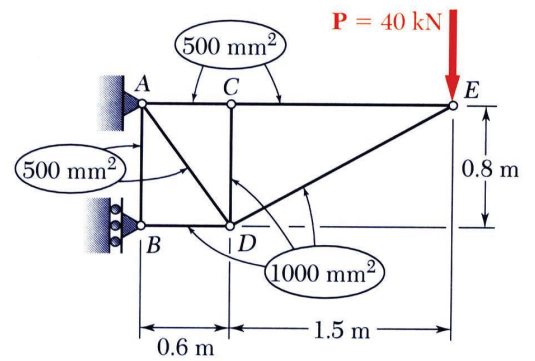
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 04

- Apply the method of joints to determine the axial force in each member.



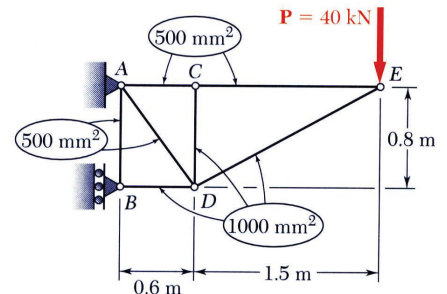
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 04

- Evaluate the strain energy of the truss due to the load  $P$ .



Member	$F_i$	$L_i, \text{m}$	$A_i, \text{m}^2$	$\frac{F_i^2 L_i}{A_i}$
AB	0	0.8	$500 \times 10^{-6}$	0
AC	$+15P/8$	0.6	$500 \times 10^{-6}$	$4\,219P^2$
AD	$+5P/4$	1.0	$500 \times 10^{-6}$	$3\,125P^2$
BD	$-21P/8$	0.6	$1000 \times 10^{-6}$	$4\,134P^2$
CD	0	0.8	$1000 \times 10^{-6}$	0
CE	$+15P/8$	1.5	$500 \times 10^{-6}$	$10\,547P^2$
DE	$-17P/8$	1.7	$1000 \times 10^{-6}$	$7\,677P^2$

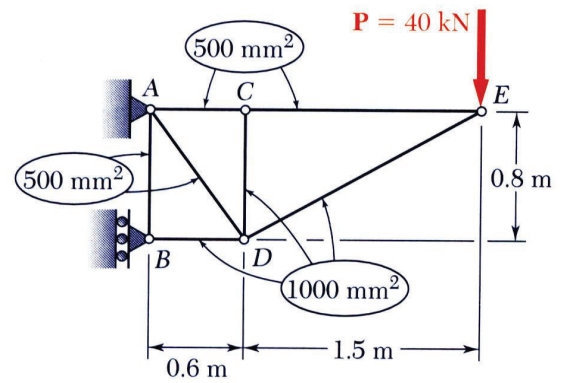
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 04

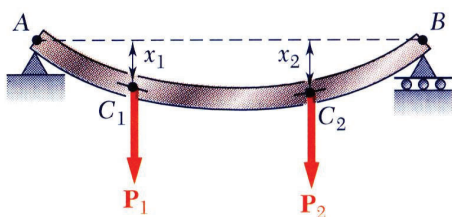
- Equate the strain energy to the work by  $P$  and solve for the displacement.



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## Energy Methods

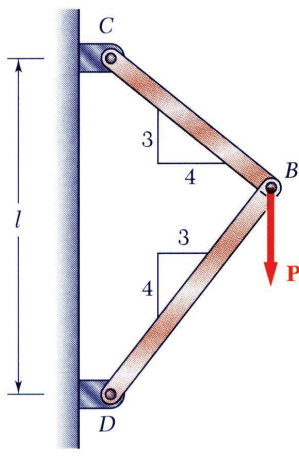
### □ Castigliano's Theorem



- In the case of a beam,

$$U = \int_0^L \frac{M^2}{2EI} dx$$

$$x_j = \frac{\partial U}{\partial P_j} = \int_0^L \frac{M}{EI} \frac{\partial M}{\partial P_j} dx$$



- For a truss,

$$U = \sum_{i=1}^n \frac{F_i^2 L_i}{2A_i E}$$

$$x_j = \frac{\partial U}{\partial P_j} = \sum_{i=1}^n \frac{F_i L_i}{A_i E} \frac{\partial F_i}{\partial P_j}$$

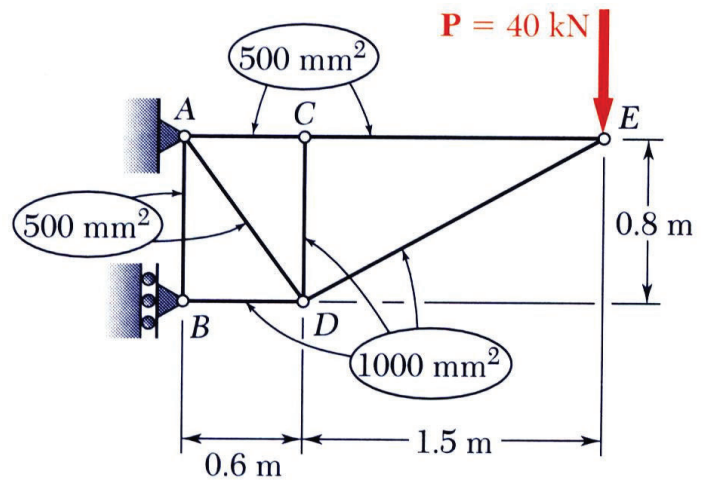
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 05

Members of the truss shown consist of sections of aluminum pipe with the cross-sectional areas indicated. Using  $E = 73 \text{ GPa}$ , determine the vertical deflection of the joint  $C$  caused by the load  $P$ .

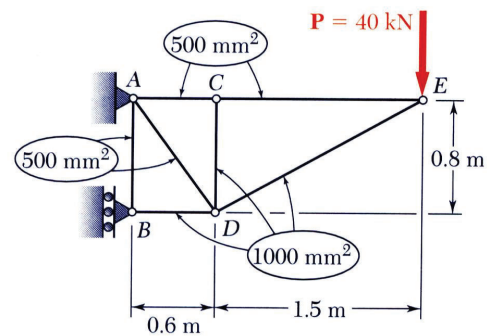


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## Energy Methods

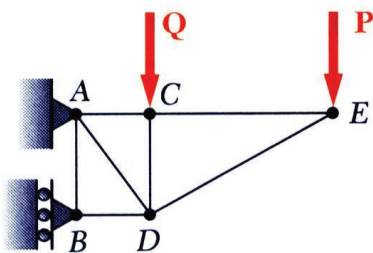
### □ Deflection Under a Single Load

#### Example 05



SOLUTION:

- Find the reactions at  $A$  and  $B$  due to a dummy load  $Q$  at  $C$  from a free-body diagram of the entire truss.



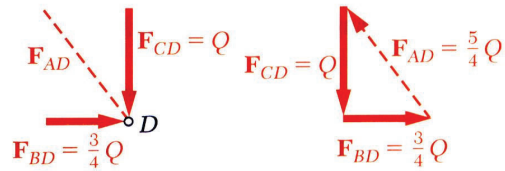
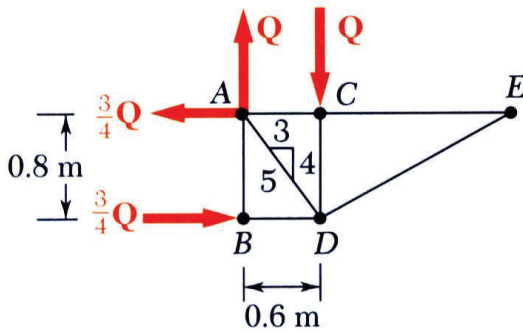
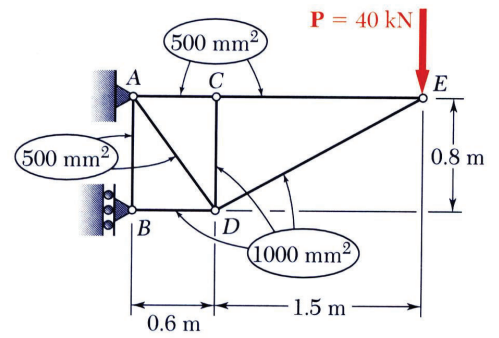
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## Energy Methods

### □ Deflection Under a Single Load

#### Example 05

- Apply the method of joints to determine the axial force in each member due to  $Q$ .

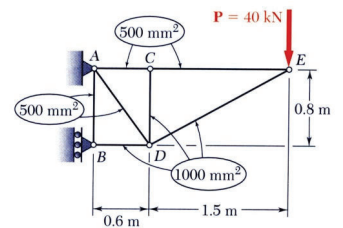


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## Energy Methods

### □ Deflection Under a Single Load

#### Example 05



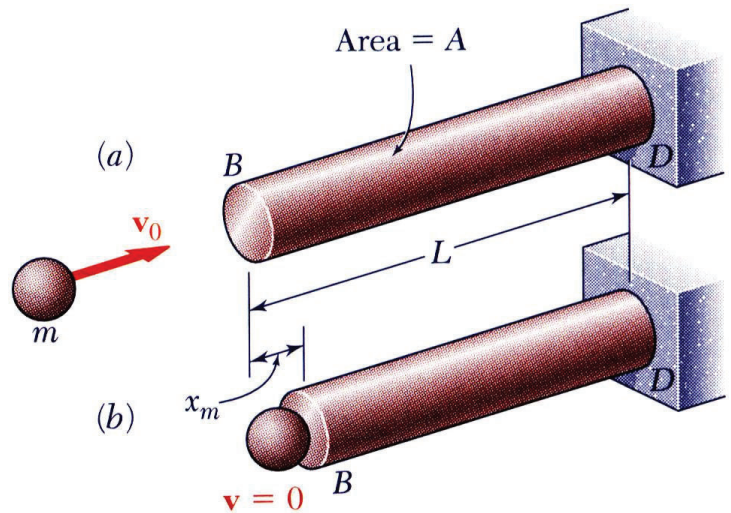
Member	$F_i$	$\partial F_i / \partial Q$	$L_i, \text{m}$	$A_i, \text{m}^2$	$\left( \frac{F_i L_i}{A_i} \right) \frac{\partial F_i}{\partial Q}$
AB	0	0	0.8	$500 \times 10^{-6}$	0
AC	$+15P/8$	0	0.6	$500 \times 10^{-6}$	0
AD	$+5P/4 + 5Q/4$	$5/4$	1.0	$500 \times 10^{-6}$	$+3125P + 3125Q$
BD	$-21P/8 - 3Q/4$	$-3/4$	0.6	$1000 \times 10^{-6}$	$+1181P + 338Q$
CD	$-Q$	-1	0.8	$1000 \times 10^{-6}$	$+800Q$
CE	$+15P/8$	0	1.5	$500 \times 10^{-6}$	0
DE	$-17P/8$	0	1.7	$1000 \times 10^{-6}$	0

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## Energy Methods

### □ Impact Loading

- Consider a rod which is hit at its end with a body of mass  $m$  moving with a velocity  $v_0$ .
- Rod deforms under impact. Stresses reach a maximum value  $\sigma_m$  and then disappear.



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## Energy Methods

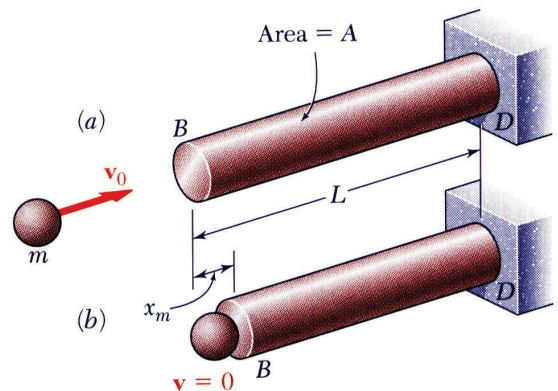
### □ Impact Loading

- To determine the maximum stress  $\sigma_m$ 
  - Assume that the kinetic energy is transferred entirely to the structure,

$$U_m = \frac{1}{2}mv_0^2$$

- Assume that the stress-strain diagram obtained from a static test is also valid under impact loading.
- Maximum value of the strain energy,

$$U_m = \int \frac{\sigma_m^2}{2E} dV$$



- For the case of a uniform rod,

$$\sigma_m = \sqrt{\frac{2U_mE}{V}} = \sqrt{\frac{mv_0^2E}{V}}$$

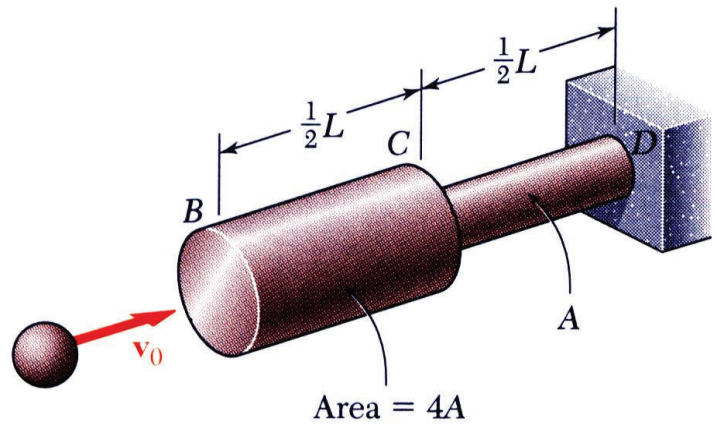
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## Energy Methods

### □ Impact Loading

#### Example 06

Body of mass  $m$  with velocity  $v_0$  hits the end of the Nonuniform rod  $BCD$ . Knowing that the diameter of the portion  $BC$  is twice the diameter of portion  $CD$ , determine the maximum value of the normal stress in the rod.



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## Energy Methods

### □ Impact Loading

#### Example 06

- Find the static load  $P_m$  which produces the same strain energy as the impact.



- Evaluate the maximum stress resulting from the static load  $P_m$



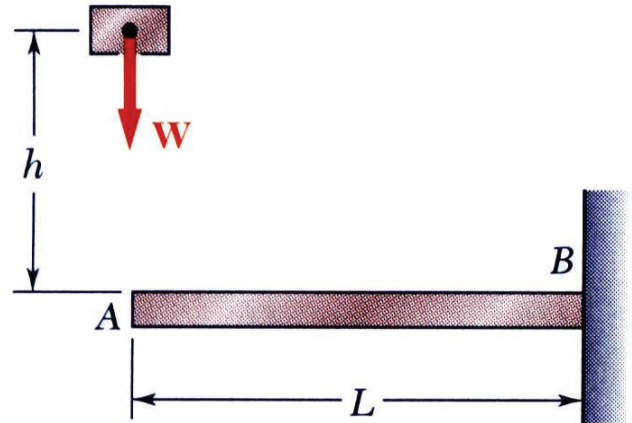
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## Energy Methods

### □ Impact Loading

#### Example 07

A block of weight  $W$  is dropped from a height  $h$  onto the free end of the cantilever beam. Determine the maximum value of the stresses in the beam.



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## Energy Methods

### □ Impact Loading

#### Example 07

- Find the static load  $P_m$  which produces the same strain energy as the impact.

For an end-loaded cantilever beam,



- Evaluate the maximum stress resulting from the static load  $P_m$



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