Mechanics of Materials



Ferdinand P.Beer, E.Russel Johnston, Jr., John T.Dewolf

Other Reference:

J.Wat Oler "Lectures notes on Mechanics od Materials" Ibrahim A.Assakkaf "Lectures notes on Mechanics od Materials"

Pure Bending

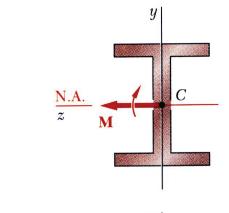
By: Kaveh Karami

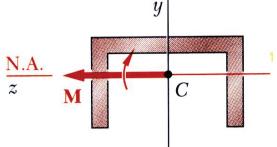
Associate Prof. of Structural Engineering

https://prof.uok.ac.ir/Ka.Karami

Pure Bending

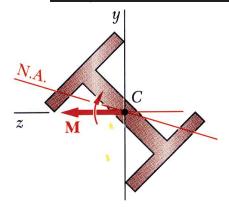


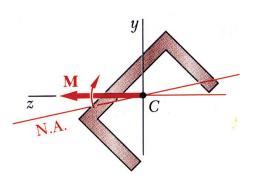




- Analysis of pure bending has been limited to members subjected to bending couples acting in a plane of symmetry.
- Members remain symmetric and bend in the plane of symmetry.
- The neutral axis of the cross section coincides with the axis of the couple

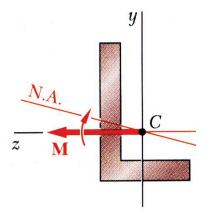
□ <u>Unsymmetric Bending</u>





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- Will now consider situations in which the bending couples do not act in a plane of symmetry.
- Cannot assume that the member will bend in the plane of the couples.
- In general, the neutral axis of the section will not coincide with the axis of the couple.

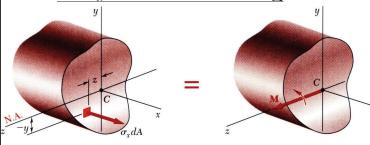


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Pure Bending

□ Unsymmetric Bending



Wish to determine the conditions under which the neutral axis of a cross section of arbitrary shape coincides with the axis of the couple as shown.

• The resultant force and moment from the distribution of elementary forces in the section must satisfy

$$F_x = M_y = 0$$
 $M_z = M = applied couple$

$$F_x = \int \sigma_x dA = 0 \quad \Rightarrow \quad \int y \, dA = 0$$

neutral axis passes through centroid

$$M_z = -\int y \sigma_x dA = M \quad \Rightarrow \boxed{\sigma_x = -\frac{My}{I}}$$

defines stress distribution

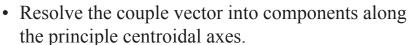
$$M_{y} = \int z \sigma_{x} dA = 0 \implies \int z \left(-\frac{y}{c} \sigma_{m} \right) dA$$

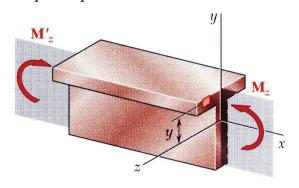
$$\Rightarrow \int yz \, dA = I_{yz} = product \ of \ inertia = 0$$

If one of y or z axis is principle then Iyz=0, so couple vector must be directed along a principal centroidal axis

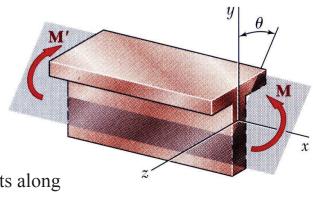
□ <u>Unsymmetric Bending</u>

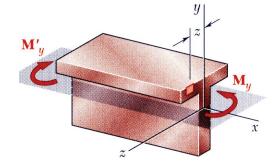
Superposition is applied to determine stresses in the most general case of unsymmetric bending.





$$M_z = M \cos \theta$$





$$M_y = M \sin \theta$$

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Pure Bending

□ <u>Unsymmetric Bending</u>

• Superpose the component stress distributions

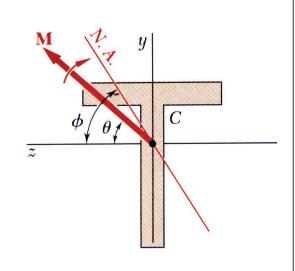
$$\sigma_x = -\frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

• Along the neutral axis,

$$\sigma_{x} = -\frac{M_{z}y}{I_{z}} + \frac{M_{y}z}{I_{y}} = 0 \implies$$

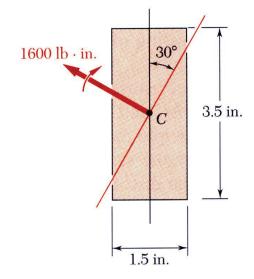
$$-\frac{(M\cos\theta)y}{I_{z}} + \frac{(M\sin\theta)z}{I_{y}} = 0$$

$$\Rightarrow \tan\phi = \frac{y}{z} = \frac{I_{z}}{I_{y}}\tan\theta$$



Example 1

A 1600 lb-in couple is applied to a rectangular wooden beam in a plane forming an angle of 30 deg. with the vertical. Determine (a) the maximum stress in the beam, (b) the angle that the neutral axis forms with the horizontal plane.

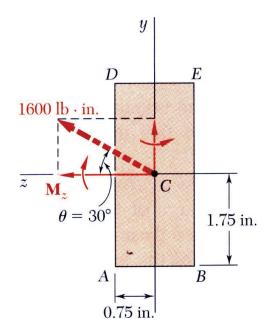


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Pure Bending

• Resolve the couple vector into components and calculate the corresponding maximum stresses.

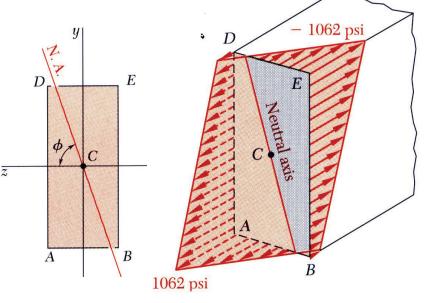
Example 1



Example 1

• The largest tensile stress due to the combined loading occurs at A.

• Determine the angle of the neutral axis.

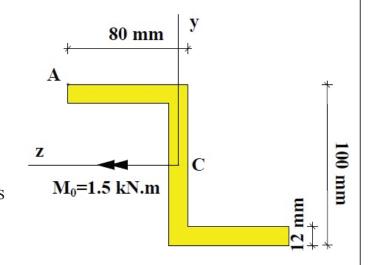


Pure Bending

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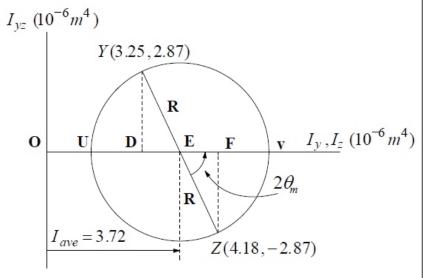
Example 2

A couple of magnitude $M_0 = 1.5 \, kN.m$ acting in a vertical plane is applied to a beam having the Z-shaped cross section shown. Determine (a) the stress at point A, (b) the angle that the neutral axis forms with the horizontal plane. The moments and product of inertia of the section with respect to the y and z axes have been computed and are as follows:



$$I_y = 3.25 \times 10^{-6} m^4$$
 $I_z = 4.18 \times 10^{-6} m^4$
 $I_{yz} = 2.87 \times 10^{-6} m^4$

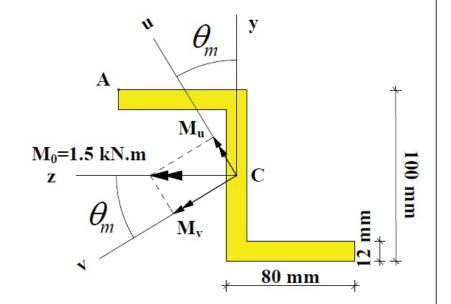
Example 2

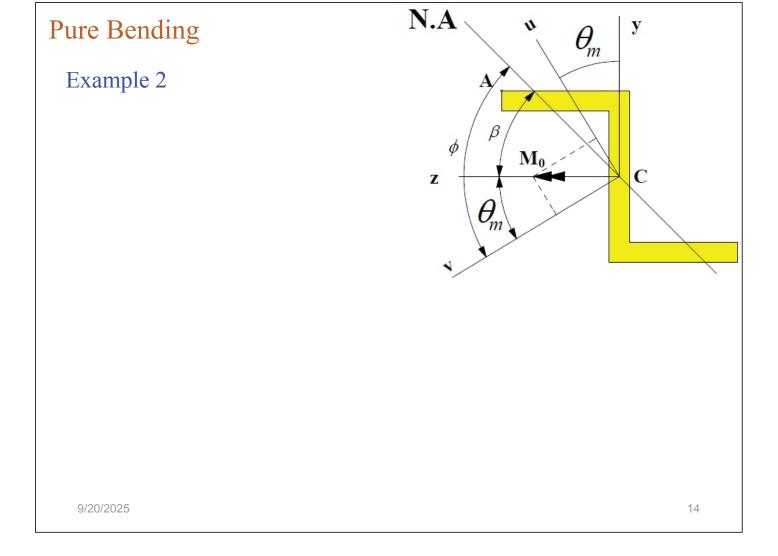


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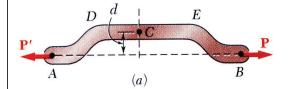
Pure Bending

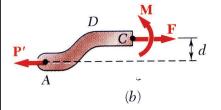
Example 2





☐ Eccentric Axial Loading in a Plane of Symmetry





• Eccentric loading

$$\sum F_x = 0 \implies F = P$$

$$\sum M_{/c} = 0 \implies M = Pd$$

 Stress due to eccentric loading found by superposing the <u>uniform stress due to a</u> <u>centric load</u> and <u>linear stress distribution due</u> <u>a pure bending moment</u>

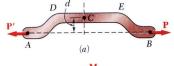
$$\sigma_x = (\sigma_x)_{\text{centric}} + (\sigma_x)_{\text{bending}}$$

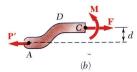
$$\Rightarrow \sigma_x = \frac{P}{A} - \frac{My}{I}$$

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Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry

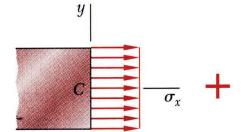


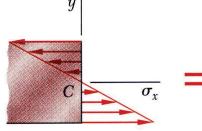


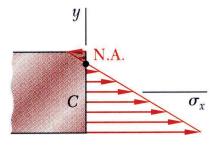
$$\sigma_{x} = \frac{P}{A} - \frac{My}{I}$$

Validity requires:

- Stresses below proportional limit
- Deformations have negligible effect on geometry
- Stresses not evaluated near points of load application.



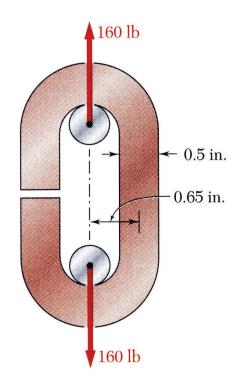




☐ Eccentric Axial Loading in a Plane of Symmetry

Example 3

An open-link chain is obtained by bending low-carbon steel rods into the shape shown. For 160 lb load, determine (a) maximum tensile and compressive stresses, (b) distance between section centroid and neutral axis

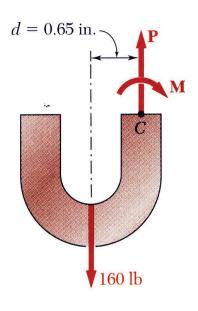


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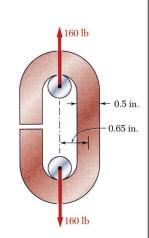
Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 3



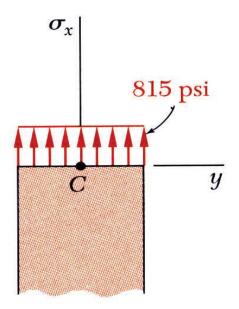
• Equivalent centric load and bending moment



☐ Eccentric Axial Loading in a Plane of Symmetry

d = 0.65 in. P M 160 lb

Example 3



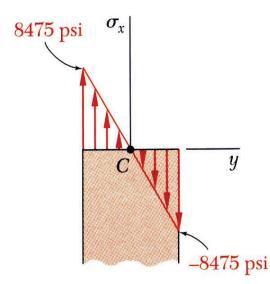
Normal stress due to a centric load

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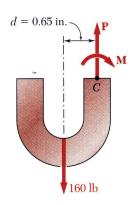
Loading combination

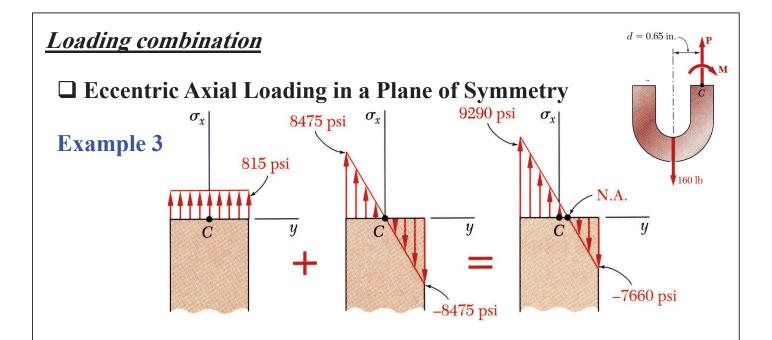
☐ Eccentric Axial Loading in a Plane of Symmetry

Example 3



• Normal stress due to bending moment



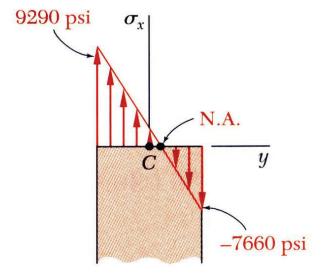


• Maximum tensile and compressive stresses

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Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry Example 3 160 lb



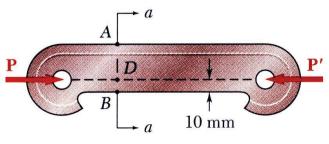
• Neutral axis location

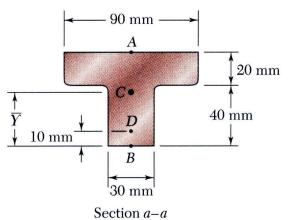
d = 0.65 in.

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 4

The largest allowable stresses for the cast iron link are 30 MPa in tension and 120 MPa in compression. Determine the largest force *P* which can be applied to the link.





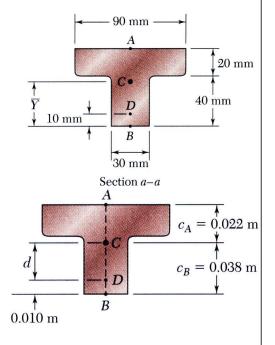
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Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 4

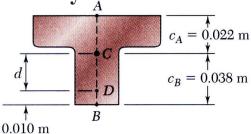
Parts	A_i	$\overline{\mathcal{Y}}_i$	$A_i \overline{y}_i$	$A_i \overline{y}_i^2$	I_{g_i}
1					
2					;



☐ Eccentric Axial Loading in a Plane of Symmetry

Example 4

• Determine an equivalent centric and bending loads.

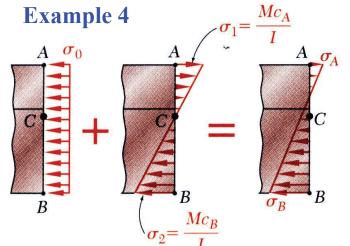


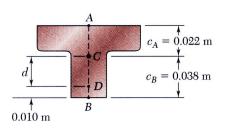
• Superpose stresses due to centric and bending loads

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Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry



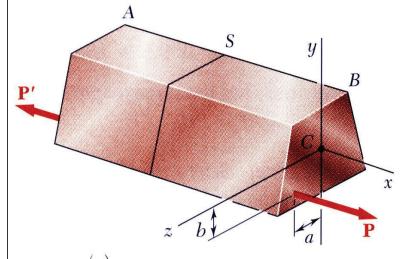


• Evaluate critical loads for allowable stresses.

• The largest allowable load



☐ General Case of Eccentric Axial Loading



• The eccentric force is equivalent to the system of a centric force and two couples.

• Consider a straight member subject to equal and opposite eccentric forces.

$$P =$$
Centric force

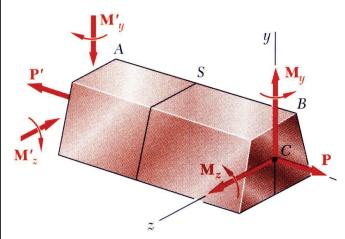
$$M_y = Pa$$

$$M_z = Pb$$

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Loading combination

☐ General Case of Eccentric Axial Loading



• By the principle of superposition, the combined stress distribution is

$$\sigma_x = \frac{P}{A} - \frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

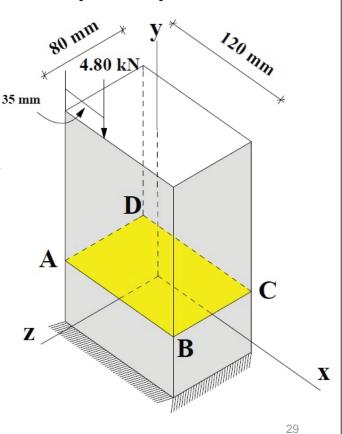
• If the neutral axis lies on the section, it may be found from

$$\frac{M_z}{I_z} y - \frac{M_y}{I_y} z = \frac{P}{A}$$

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 5

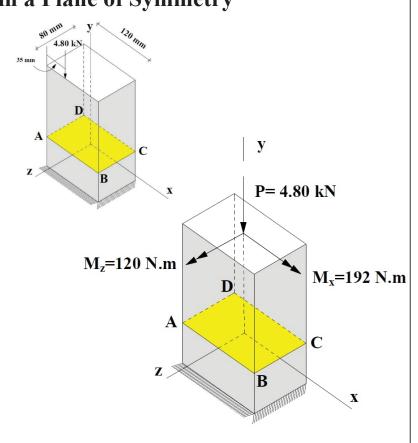
A vertical 4.80 kN load is applied as shown on a wooden post of rectangular cross section, 80 by 120 mm. (a) Determine the stress at points A, B, C, and D. (b) Locate the neutral axis of the cross section.

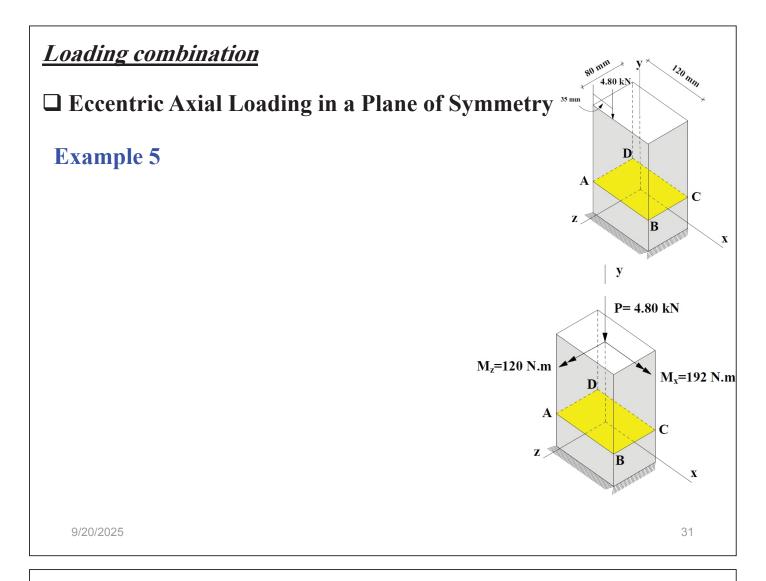


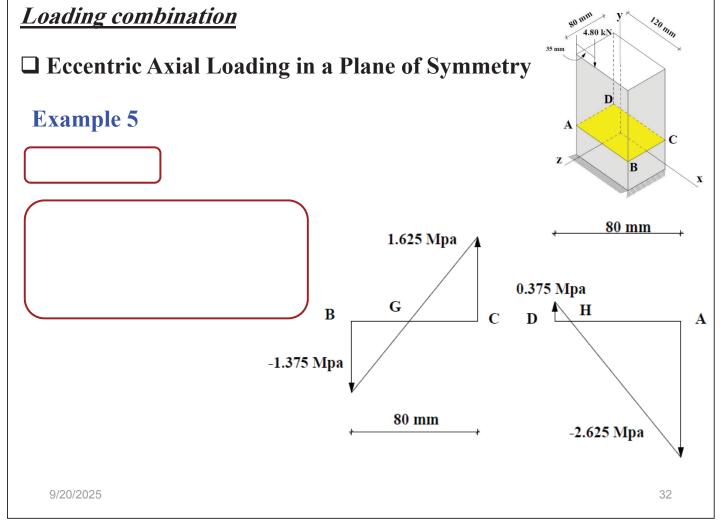
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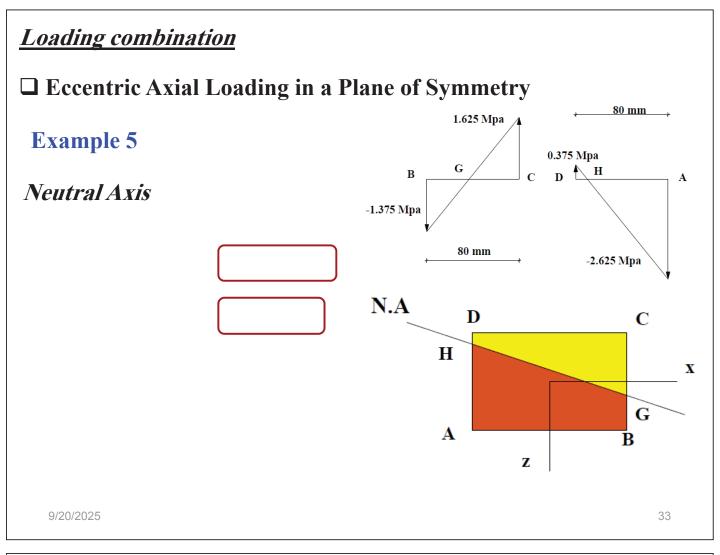
Loading combination☐ Eccentric Axial Loading in a Plane of Symmetry

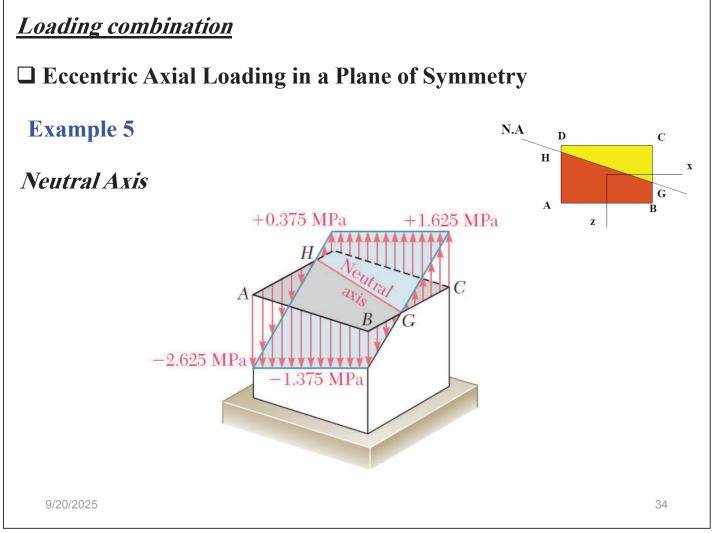
Example 5











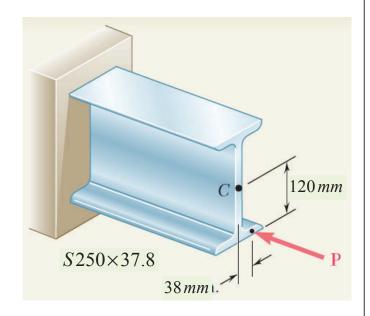
☐ Eccentric Axial Loading in a Plane of Symmetry

Example 6

A horizontal load P is applied as shown to a short section of an S250 X 37.8 rolled-steel member. Knowing that the compressive stress in the member is not to exceed 82 MPa, determine the largest permissible load P.

$$A = 4820mm^{2}$$

$$S_{x} = 402 \times 10^{3} mm^{3} \quad S_{y} = 47.5 \times 10^{3} mm^{3}$$

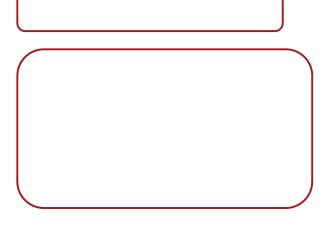


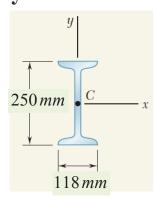
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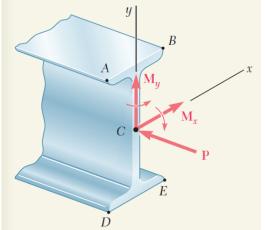
Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 6





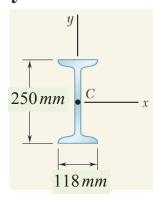


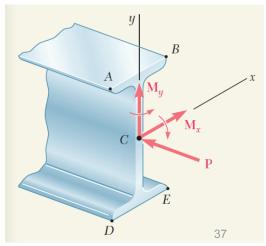
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☐ Eccentric Axial Loading in a Plane of Symmetry

Example 6



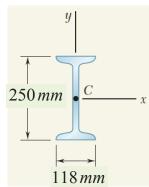


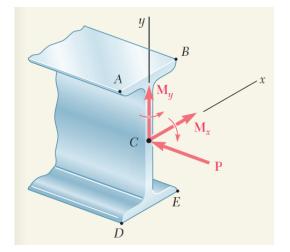
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Loading combination

☐ Eccentric Axial Loading in a Plane of Symmetry

Example 6





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